

HONTSBURG N. & S.
CENTER ROAD.

W. Booth

LEVEL BOOK

743

TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.
1/16	.0052	1 1/16	.1094	5 1/16	.4219	6 1/16	.5260	7 1/16	.6302	8 1/16	.7344	9 1/16	.8385	10 1/16	.9427	11 1/16	.0469	12 1/16	.1510
2/16	.0104	2 1/16	.1146	6 1/16	.4271	7 1/16	.5313	8 1/16	.6354	9 1/16	.7396	10 1/16	.8438	11 1/16	.9479	12 1/16	.0521	13 1/16	.1563
3/16	.0156	3 1/16	.1198	7 1/16	.4323	8 1/16	.5365	9 1/16	.6406	10 1/16	.7448	11 1/16	.8490	12 1/16	.9531	13 1/16	.0573	14 1/16	.1615
4/16	.0208	4 1/16	.1250	8 1/16	.4375	9 1/16	.5417	10 1/16	.6458	11 1/16	.7500	12 1/16	.8542	13 1/16	.9583	14 1/16	.0625	15 1/16	.1667
5/16	.0260	5 1/16	.1302	9 1/16	.4427	10 1/16	.5469	11 1/16	.6510	12 1/16	.7552	13 1/16	.8594	14 1/16	.9635	15 1/16	.0677	16 1/16	.1719
6/16	.0313	6 1/16	.1354	10 1/16	.4479	11 1/16	.5521	12 1/16	.6563	13 1/16	.7604	14 1/16	.8646	15 1/16	.9687	16 1/16	.0729	17 1/16	.1761
7/16	.0365	7 1/16	.1406	11 1/16	.4531	12 1/16	.5573	13 1/16	.6615	14 1/16	.7656	15 1/16	.8698	16 1/16	.9739	17 1/16	.0781	18 1/16	.1823
8/16	.0417	8 1/16	.1458	12 1/16	.4583	13 1/16	.5625	14 1/16	.6667	15 1/16	.7708	16 1/16	.8750	17 1/16	.9791	18 1/16	.0833	19 1/16	.1875
9/16	.0469	9 1/16	.1510	13 1/16	.4635	14 1/16	.5677	15 1/16	.6719	16 1/16	.7760	17 1/16	.8802	18 1/16	.9843	19 1/16	.0885	20 1/16	.1927
10/16	.0521	10 1/16	.1563	14 1/16	.4688	15 1/16	.5729	16 1/16	.6771	17 1/16	.7813	18 1/16	.8854	19 1/16	.9895	20 1/16	.0938	21 1/16	.1979
11/16	.0573	11 1/16	.1615	15 1/16	.4740	16 1/16	.5781	17 1/16	.6823	18 1/16	.7865	19 1/16	.8906	20 1/16	.9947	21 1/16	.0990	22 1/16	.2031
12/16	.0625	12 1/16	.1667	16 1/16	.4792	17 1/16	.5833	18 1/16	.6875	19 1/16	.7917	20 1/16	.8958	21 1/16	.9999	22 1/16	.1042	23 1/16	.2083
13/16	.0677	13 1/16	.1719	17 1/16	.4844	18 1/16	.5885	19 1/16	.6927	20 1/16	.7969	21 1/16	.9010	22 1/16	.0051	23 1/16	.1094	24 1/16	.2125
14/16	.0729	14 1/16	.1771	18 1/16	.4896	19 1/16	.5938	20 1/16	.6979	21 1/16	.8021	22 1/16	.9062	23 1/16	.0104	24 1/16	.1135	25 1/16	.2166
15/16	.0781	15 1/16	.1823	19 1/16	.4948	20 1/16	.5990	21 1/16	.7031	22 1/16	.8073	23 1/16	.9114	24 1/16	.0156	25 1/16	.1187	26 1/16	.2208
16/16	.0833	16 1/16	.1875	20 1/16	.5000	21 1/16	.6042	22 1/16	.7083	23 1/16	.8125	24 1/16	.9166	25 1/16	.0208	26 1/16	.1239	27 1/16	.2269
17/16	.0885	17 1/16	.1927	21 1/16	.5052	22 1/16	.6094	23 1/16	.7135	24 1/16	.8177	25 1/16	.9218	26 1/16	.0260	27 1/16	.1291	28 1/16	.2320
18/16	.0938	18 1/16	.1979	22 1/16	.5104	23 1/16	.6146	24 1/16	.7188	25 1/16	.8229	26 1/16	.9270	27 1/16	.0313	28 1/16	.1344	29 1/16	.2351
19/16	.0990	19 1/16	.2031	23 1/16	.5156	24 1/16	.6198	25 1/16	.7240	26 1/16	.8281	27 1/16	.9322	28 1/16	.0365	29 1/16	.1396	30 1/16	.2383
20/16	.1042	20 1/16	.2083	24 1/16	.5208	25 1/16	.6250	26 1/16	.7292	27 1/16	.8333	28 1/16	.9375	29 1/16	.0417	30 1/16	.1448	31 1/16	.2414

B. K. ELLIOTT COMPANY, PITTSBURG, PA.

DRAWING MATERIALS AND SURVEYING INSTRUMENTS

Huntsburg N. & S. Center Road. 5R528

112

3-12-21
Cloudy
muddy
warm

Hanna
Grad

Sta.	B.S.	H. I.	F.S.	Elev
B.M.	12.24	1120.45		1108.21
T.P.	10.12	1130.02	0.55	1119.90
B.M.			8.37	1121.65
T.P.	12.91	1139.57	3.36	1126.66
B.M.			3.40	1136.17
T.P.	13.05	1149.45	3.17	1136.10
T.P.	11.20	1159.64	1.01	1148.74
B.M.			1.08	1158.56
T.P.	6.87	1163.21	3.30	1156.34
B.M.			8.72	1154.19
T.P.	9.36	1168.94	3.63	1159.59
T.P.	4.14	1172.01	1.07	1167.87
B.M.			2.03	1169.98
T.P.	1.20	1167.78	5.43	1166.58
T.P.	0.33	1158.69	9.42	1158.36
x B.M.	0.44	1153.79	5.34	1153.35
T.P.	4.73	1157.28	1.24	1152.55
B.M.			7.22	1150.06
T.P.	12.38	1169.10	0.56	1156.72
T.P.	10.76	1179.39	0.47	1168.63
x B.M.			5.67	1173.72
T.P.	12.05	1190.79	0.65	1178.74
T.P.	11.67	1202.25	0.21	1190.58

✓

BENCH MARKS

2 nails W. root 20" Hickory 40' Rt. Sta 0-

x on S.W. cor. W. Head Wall Corn. Culv. Sta. 12+00

1 tack on S.E. root 30" Maple 35' Lt. Sta. 20+40

1 tack on N. root, 13" Maple 25' Lt. Sta. 31+50

x on N.W. cor. W. Head Wall, Corn. Culv. Sta. 4+50

" " " " " " " " " " Sta. 4

Nail on S.E. root 15" Maple 25' Lt. Sta. 57+10

Nail on E. root 20" Maple 'Lt. Sta. 68+30

x on S.W. Cor. W. Head Wall Stone Culv. Sta. 80+73

Nail on W. root 24" Maple 'Rt. Sta. 88+48
88±

1202 25

T.P. 12.66 1214 82 0.09 1202.16

B.M. 1.75 1213.07 Nail in W. root 24" Evergreen 40' Rt. Sta. 100+10

T.P. 12.07 1226 52 0.32 1214.50

T.P. 12.20 1238 55 0.17 1226.35

T.P. 11.53 1250.04 0.04 1238.51

T.P. 11.23 1260 80 0.47 1249.57

x B.M. 4.30 1256.50 Nail in W. Root 60" Elm 35' Rt., Sta. 110+25

T.P. 6.32 1265 52 1.60 1259.20

x B.M. 5.96 1259.56 x on SW. Cor. Corr. Porch to store
1260.20

CROSS-SECTIONS

3-16-'21
windy !!!
cold
Mud !!!!
Fair

Hanna
Grou
Thrasher

Sta. B.S. H. I. F.S. Elev.

B.M. 12.16 1120⁺ 37 1108.21

0 10.2 10.2

1 9.8 10.6

+25 10" C.I. Pipe (sec.) Culvert
[Req: 12"] 10.0 10.4

2 9.5 10.9

3 8.6 11.8

4 6.5 13.9

5 3.4 17.0

T.P. 786 1127.76 0.47 1119.90

6 6.5 21.3

w. root 20" Hickory 40' Rt, Sta. 0—

+1.4 +0.1 0.0 -0.9 -0.1 -0.2
3.8 10.1 10.2 11.1 10.3 10.4
2.5 11 1.5 1.6 2.5

+2.0 +1.4 -1.2 -0.2 0.0 -0.5 -1.8 -2.0 -1.2
7.8 8.7 11.0 10.0 9.2 10.3 11.6 11.8 11.0
2.5 1.7 11-9 7 1.0 1.2 1.6 2.5

+1.8 +1.4 -1.0 -2.3 -0.2 0.0 -0.4 -2.6 -3.2
8.2 8.6 11.0 12.3 10.2 10.0 10.4 12.2 13.2
2.5 1.9 1.3 8 7 9 1.6 2.5

← 7' × 9' →

+1.6 +1.1 -0.4 0.0 -1.0 -1.6
7.5 8.4 9.9 9.5 10.5 11.1
2.5 1.7 1.3 1.1 2.5

+0.8 +0.5 -0.3 0.0 -0.3 -1.1 -2.1
7.8 8.1 8.7 8.6 8.7 9.7 10.7
2.5 1.6 1.1 1.1 1.4 2.5

+0.7 +0.4 0.0 -0.6 0.0 -0.3 -0.7 -0.5
5.8 6.1 6.5 7.1 6.5 6.8 7.2 7.0
2.5 1.6 15-12 1.1 1.5 1.7 1.3 2.5

+2.5 +2.2 -0.1 1.0 -0.4 0.0 -0.5 -0.8 +1.2 +1.0
0.9 1.2 3.5 4.4 3.8 3.4 3.9 4.2 2.2 2.4
2.5 1.8 1.4 10-9 8 7 9 1.3 2.5

+2.7 +2.1 0.0 -1.4 -0.7 0.0 -0.3 -0.8 +0.5 +0.4
3.8 4.1 6.5 7.4 7.2 6.5 6.0 7.3 6.0 6.1
2.5 1.7 14-11 1.0 1.8 1.5 1.3 1.1 2.5

1127 ^B 7C

6+50

4.2 23.6

+2.2	+1.4	-0.7	-1.2	-0.4	0.0	-0.4	-1.1	-0.6	-1.1
2.0	2.8	4.9	5.4	4.6	4.2	4.4	5.3	4.8	5.3
<u>2.5</u>	<u>1.5</u>	<u>13</u>	<u>10</u>	<u>9</u>	<u>7</u>	<u>5</u>	<u>7</u>	<u>8</u>	<u>2.5</u>

7

3.3 24.5

+1.2	+0.6	-0.1	-1.0	-0.1	0.0	-0.8	-1.0	-1.8
2.1	2.7	3.9	4.3	3.7	3.3	4.1	4.3	5.1
<u>2.5</u>	<u>1.7</u>	<u>1.5</u>	<u>1.1</u>	<u>9</u>	<u>9</u>	<u>5</u>	<u>1.6</u>	<u>20-2.5</u>

8

2.4 25.4

+0.8	-0.8	-0.1	0.0	-0.9	-0.3	-0.8
1.6	3.2	2.5	2.4	3.3	2.7	3.2
<u>2.5</u>	<u>2.0</u>	<u>1.2</u>	<u>9</u>	<u>5</u>	<u>1.3</u>	<u>2.5</u>

9

1.7 26.1

T.P. 3.20 1130 17 0.79 1126.97

+0.8	-0.2	-1.0	-0.2	0.0	-0.6	+0.1	+0.3
0.9	1.9	2.7	1.9	1.7	2.3	1.6	1.4
<u>2.5</u>	<u>1.4</u>	<u>1.2</u>	<u>9</u>	<u>5</u>	<u>1.5</u>	<u>2.5</u>	

9+50

3.0 26.6

+1.7	-0.4	-1.1	-0.1	0.0	-0.1	+0.9	+1.5
1.2	4.0	4.7	3.7	3.6	3.7	2.7	2.1
<u>2.5</u>	<u>2.2</u>	<u>1.3</u>	<u>1.2</u>	<u>1.0</u>	<u>8</u>	<u>1.2</u>	<u>2.5</u>

10

5.0 25.2

+2.5	+1.9	0.0	-1.3	-0.6	0.0	-0.1	-0.7	+2.1	+2.6
2.5	3.1	5.0	6.3	5.6	5.0	5.1	5.7	2.9	2.4
<u>2.5</u>	<u>1.8</u>	<u>1.4</u>	<u>1.1</u>	<u>1.0</u>	<u>5.0</u>	<u>4</u>	<u>5</u>	<u>1.1</u>	<u>2.5</u>

11

10.6 19.6

Banks end at +80

-0.5	-0.2	-0.8	0.0	-1.2	-1.6
1.1	10.8	11.4	10.6	11.8	12.2
<u>2.5</u>	<u>1.2</u>	<u>1.0</u>	<u>1.0</u>	<u>1.3</u>	<u>2.5</u>

12

stone
Exc. sand
Culvert 10.2 20.0

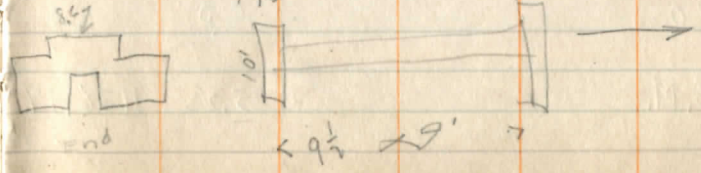
4x3 1/2

Exc. sand

OK

Top cover 10.4 19.8

-3.8	-4.5	-0.1	0.0	-0.1	-5.0	-5.1
1.0	1.4	10.3	10.2	10.3	15.3	15.3
<u>2.2</u>	<u>10.4</u>	<u>9.3</u>	<u>9</u>	<u>9</u>	<u>10</u>	<u>2.5</u>



1130² 17

B.M.

8.53

1121.64^{.65}

+ on Lt Parapet

13

9.5

20.7

$$\begin{array}{ccccccc} -1.5 & -0.1 & -0.4 & 0.0 & -0.4 & -0.7 & +0.3 \\ \hline 11.0 & 9.4 & 9.9 & 9.5 & 9.9 & 10.2 & 9.2 \\ \hline 25 & 11 & 9 & & 9 & 17 & 25 \end{array} \quad \checkmark$$

14

4.7

25.5

T.P.

11.58

11.38

20

3.55

1126.62

$$\begin{array}{ccccccccccc} +2.7 & +1.6 & -1.0 & -0.4 & 0.0 & -0.4 & -1.3 & +2.3 & +3.3 & +3.7 \\ \hline 2.0 & 3.1 & 5.7 & 5.1 & 4.7 & 5.1 & 6.0 & 2.4 & 1.4 & 1.0 \\ \hline 25 & 15 & 9 & 7 & & 4 & 7 & 13 & 19 & 25 \end{array} \quad \checkmark$$

15

7.2

31.0

$$\begin{array}{ccccccc} +0.7 & -1.0 & -0.4 & 0.0 & -0.2 & -1.0 & +1.3 & +2.7 \\ \hline 6.5 & 8.2 & 7.6 & 7.2 & 7.4 & 8.2 & 5.9 & 4.5 \\ \hline 25 & 14 & 9 & 8 & 5 & 2-8 & 12 & 21-25 \end{array} \quad \checkmark$$

16

3.7

34.5

$$\begin{array}{ccccccc} -1.4 & -0.7 & -1.3 & -0.5 & 0.0 & -0.8 & 0.0 & +1.5 \\ \hline 5.3 & 4.4 & 5.0 & 4.2 & 3.7 & 4.5 & 3.7 & 2.2 \\ \hline 25 & 11 & 9 & 7 & & 7 & 9 & 20-25 \end{array} \quad \checkmark$$

17

2.2

36.0

T.P.

3.89

11.41

5.5

0.54

1137.66

$$\begin{array}{ccccccc} -1.4 & -0.5 & -0.8 & -0.2 & 0.0 & -0.3 & -0.7 & -0.4 & +1.4 \\ \hline 3.6 & 2.7 & 3.0 & 2.4 & 2.2 & 2.5 & 2.7 & 2.6 & 0.8 \\ \hline 25 & 11 & 9 & 7 & & 5 & 7 & 8 & 25 \end{array} \quad \checkmark$$

18

3.0

38.6

$$\begin{array}{ccccccc} -1.3 & -0.7 & -1.2 & -0.4 & 0.0 & -0.4 & -1.0 & -0.4 & 0.0 \\ \hline 4.3 & 3.7 & 4.2 & 3.4 & 3.0 & 3.4 & 4.0 & 3.4 & 3.0 \\ \hline 25 & 11 & 9 & 7 & & 5 & 6 & 7 & 25 \end{array} \quad \checkmark$$

19

6.3

35.3

$$\begin{array}{ccccccc} -0.9 & -0.5 & -0.9 & -0.3 & 0.0 & -0.5 & +1.3 & +2.7 \\ \hline 7.2 & 6.8 & 7.3 & 6.6 & 6.3 & 6.8 & 5.0 & 3.6 \\ \hline 25 & 9 & 8 & 7 & & 6 & 13 & 25 \end{array} \quad \checkmark$$

20

8.0

33.6

$$\begin{array}{ccccccc} 0.0 & -0.5 & -0.8 & 0.0 & -0.3 & -1.0 & -0.8 \\ \hline 8.0 & 8.5 & 8.8 & 8.0 & 8.2 & 9.0 & 8.3 \\ \hline 25 & 18 & 10 & 7 & 10 & 25 \end{array} \quad \checkmark$$

B.M.

5.38

1136.17

Maple 35' Lt. Sta 20+40

✓

1141.55

21 8.8 32.8

~~F.P.~~

+72 Stone Culvert 8.5 33.1

2' x 2'

Poor cond.
(Reqd. 2x2' Box)

22 7.9 33.7

+40 5.3 36.3

T.P. 13.07 1151.84 2.78 1138.77

23 10.1 41.7

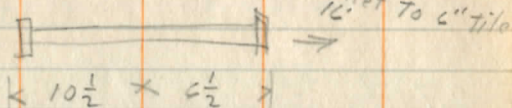
24 3.5 48.3

+25 3.3 48.5

25 6.2 45.6

+1.9 +1.7 -1.2 -0.2 0.0 -0.1 -1.4 -1.0 -1.7 ✓
 $\frac{6.9}{25} \frac{7.4}{14} \frac{10.0}{7} \frac{9.0}{5} \frac{8.8}{5} \frac{8.9}{7} \frac{10.2}{10} \frac{9.8}{18} \frac{10.5}{25}$

-3.3 -4.2 0.0 0.0 -0.4 -5.5 -5.3 -4.4
 $\frac{11.8}{25} \frac{12.7}{11} \frac{5.5}{10} \frac{3.5}{5} \frac{8.9}{6} \frac{14.0}{7} \frac{3.8}{12} \frac{12.8}{25}$



-1.6 -0.5 -0.9 +0.1 0.0 -0.3 -1.4 -3.1 -3.3 ✓
 $\frac{9.5}{25} \frac{8.4}{21} \frac{8.8}{14} \frac{7.8}{10} \frac{7.9}{5} \frac{8.7}{3} \frac{9.3}{5} \frac{11.0}{15} \frac{11.3}{25}$

+2.9 0.0 -0.3 0.0 +0.2 -0.5 +1.7 +2.5
 $\frac{2.4}{25} \frac{5.3}{12} \frac{5.6}{10} \frac{5.3}{5} \frac{5.1}{5} \frac{5.8}{6} \frac{3.6}{12} \frac{2.8}{25}$

+4.9 +4.7 -0.5 0.0 -0.4 +4.1 +4.5 ✓
 $\frac{5.2}{25} \frac{5.7}{13} \frac{10.6}{2} \frac{10.1}{2} \frac{10.5}{2} \frac{6.0}{13} \frac{5.6}{25}$

+1.2 +0.6 -0.9 0.0 -1.0 -0.4 +0.2 0.0 ✓
 $\frac{2.3}{25} \frac{2.9}{12} \frac{4.4}{8} \frac{3.5}{5} \frac{4.5}{9} \frac{3.7}{10} \frac{3.3}{16} \frac{3.5}{25}$

+0.7 +0.4 -1.0 0.0 -1.2 -0.5 +0.2 -0.2
 $\frac{2.6}{25} \frac{2.9}{12} \frac{4.3}{8} \frac{3.3}{5} \frac{4.5}{9} \frac{3.8}{10} \frac{3.1}{19} \frac{3.5}{25}$

+2.8 +2.3 0.0 -0.5 0.0 -0.4 -1.3 +0.5 ✓
 $\frac{3.4}{25} \frac{3.9}{15} \frac{6.2}{12} \frac{6.7}{10} \frac{6.2}{6} \frac{6.6}{6} \frac{7.5}{2} \frac{5.7}{14} -25$

115184

26 12.4 39.4

T.P. 0.92 1140.50 122.6 1139.58

+75 55 35.0

27 6.3 34.2

+67 E Stone Culvert 6.0 33.9

3 1/2 x 2

Poor cond.

(Reqd Con BBL. stone Hd. walls.)

28 5.9 34.6

+40 4.3 36.2

T.P. 13.12 1150.90 2.72 1137.78

29 12.1 38.8

30 3.6 47.3

M.M.

T.P. 9.46 1159.71 0.65 1150.25

+3.2	+2.6	+0.2	-0.8	0.0	-0.9	+1.6	+1.8	✓
9.2	98	122	132	124	13.3	108	106	
25	17	14	11		4	10	25	

+3.0	-0.3	0.0	-1.0	0.0	+0.8	+4.5		
2.5	5.8	5.5	6.5	5.5	4.7	5.0		
25	18	12	2	4	7	25		

+0.1	-0.1	-0.6	0.0	-0.5	-2.2	-2.8	✓	
6.2	6.4	6.7	6.3	6.8	8.5	7.1		
25	16	14	4	15	25			

-3.7	-3.7	+0.8	-0.2	0.0	0.0	+0.6	-3.3	-3.5
10.3	10.3	5.8	6.3	6.6	6.6	5.8	10.5	10.1
22	15	7	13	6	3	5	6	25

18"



< 15' x 5'-3" >

-1.1	-0.4	-0.7	-0.1	0.0	-0.2	-2.4	-3.0	✓
7.0	6.3	6.6	6.0	5.9	6.1	8.3	8.9	
25	19	17	15	6	12	25		

-0.7	-0.6	0.0	-0.7	-0.2	+0.6			
5.0	4.9	4.3	5.0	4.5	3.7			
25	13	3	5-12	16	-25			

+3.4	+0.1	-0.9	-0.1	0.0	-0.7	+0.1	+4.7	✓
8.7	12.0	13.0	12.3	12.1	12.8	12.0	7.4	
25-20	15-14	13	11	3	7	17	-25	

+3.6	-0.6	0.0	0.0	-0.8	+2.5	+4.5	✓	
0.0	4.2	3.6	3.6	4.1	1.1	2.1		
25-21	11	12	3.6	2	9	25		

P.M.

1159 71

30+90

7.8 51.9

31

7.3 52.4

+ CL₁ Rd Rt,
" " Lt,

6.8 52.9

6.8 52.9

(Grain water in ditch of Rd to R²L¹L¹)

+45

5.7 54.5

32

3.4 56.3

B.M.

6.4 1153.57

33

5.3 54.4

34

5.5 54.2

T.P. 4.06 1156 8 C

6.91 1152.80

35

4.6 52.3

+85 4.2 " C.L.P. (sec)
(R edg new)

4.8 52.1

+0.9	+0.2	0.0	-0.7	+0.5	+0.2
6.9	7.6	7.8	8.5	7.3	7.6
<u>25</u>	<u>13</u>		<u>10</u>	<u>14</u>	<u>2.5</u>

same ↑ ↑
7.3 10.1
25

0.0	-0.2	-1.9	-6.5
6.8	7.0	8.7	13.3
<u>13</u>	<u>25</u>	<u>7.5</u>	

-5.1	+0.7
11.9	6.1
<u>100</u>	<u>25</u>

+2.7	+2.4	-0.8	0.0	-3.0	+0.5
2.5	2.8	6.0	5.2	8.7	4.7
<u>25</u>	<u>21</u>	<u>13</u>		<u>21</u>	<u>30</u>

+2.2	+1.8	-1.0	0.0	-0.4	-1.1	+0.5	-0.1
1.2	1.6	4.4	3.7	3.8	4.5	2.9	3.5
<u>25</u>	<u>16</u>	<u>11</u>		<u>10</u>	<u>15</u>	<u>19</u>	<u>25</u>

25' Lt. 314 50 N. root 18" Maple.

+0.5	-0.5	-0.8	0.0	-1.1	-2.1
4.8	5.2	6.1	5.3	6.4	7.4
<u>25</u>	<u>11</u>	<u>7</u>		<u>14</u>	<u>25</u>

+2.7	+2.0	-1.2	0.0	-0.1	-0.7	-0.3	-1.0	-0.4
2.8	3.5	6.7	5.5	5.6	6.2	5.8	6.5	5.9
<u>25</u>	<u>15</u>	<u>9</u>		<u>11</u>	<u>16</u>	<u>18</u>	<u>20</u>	<u>25</u>

+1.8	+1.1	-0.8	0.0	-1.0	-1.4
2.8	3.5	5.4	4.6	5.6	6.0
<u>25</u>	<u>18</u>	<u>15</u>		<u>15-1.9</u>	<u>25</u>

-0.7	-1.3	-0.4	0.0	-0.5	-1.6	-1.3	-2.2
5.5	6.1	5.2	4.8	5.3	6.4	6.1	7.0
<u>20</u>	<u>3</u>	<u>7</u>		<u>13</u>	<u>14</u>	<u>25</u>	<u>40</u>

class outlet

1156⁹ 86

36

4.6 52.3

0.0 -0.7 -0.7 0.0 -0.3 -1.1 -0.8 -1.3 ✓
 $\frac{4.6}{25} \frac{55}{17} \frac{5.3}{9} \frac{4.6}{11} \frac{4.9}{15} \frac{5.7}{16} \frac{5.7}{25}$

37

3.1 53.8

-0.6 -1.0 -0.5 0.0 -0.3 -0.9 +1.3 +1.6 ✓
 $\frac{3.7}{25} \frac{4.1}{17} \frac{3.6}{12} \frac{3.1}{10} \frac{3.4}{14} \frac{4.0}{21} \frac{1.8}{25} \frac{1.6}{25}$

T.F.

7.19 1163 66

0.39 1156.47

38

6.7 57.0

+3.6 +3.3 -0.1 0.0 +0.6 +2.8 ✓
 $\frac{3.1}{25} \frac{3.7}{22} \frac{6.8}{13} \frac{6.7}{10} \frac{6.1}{10} \frac{4.3}{25}$

+75

3.3 60.4

+2.5 +0.8 0.0 0.0 +0.4 ✓
 $\frac{0.8}{25} \frac{2.5}{18} \frac{3.3}{17} \frac{3.3}{17} \frac{2.7}{21-25}$

39

3.4 60.3

+2.4 +0.6 0.0 -0.2 +0.9 ✓
 $\frac{1.0}{25} \frac{2.8}{18} \frac{3.4}{18} \frac{3.6}{18} \frac{2.5}{20-25}$

40

7.8 55.9

+3.2 +1.8 +0.2 -1.0 -0.4 0.0 -0.3 -0.9 +0.3 +2.5 ✓
 $\frac{4.6}{25} \frac{6.0}{17} \frac{7.6}{12} \frac{8.8}{11} \frac{8.2}{6} \frac{7.8}{12} \frac{8.1}{12} \frac{8.7}{15} \frac{7.5}{18} \frac{5.5}{23-25}$

41

10.7 53.6

+0.8 -0.6 -0.2 0.0 -0.2 -0.6 -1.1 ✓
 $\frac{9.3}{25} \frac{10.7}{16} \frac{10.3}{10.8} \frac{10.1}{15} \frac{10.3}{15} \frac{10.7}{18} \frac{11.5}{25}$

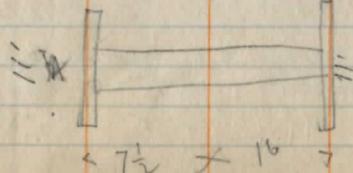
B.M.

+40

♀ Con Box **CULT** 98
 3x 2'-3" Good Cond
 con. floor
 (Ext. Lt. end)

9.7 53.9

-3.4 -4.0 +0.6 +0.1 0.0 0.0 +0.5 -4.8 4.7 ✓
 $\frac{13.2}{16} \frac{13.3}{Fl} \frac{9.6}{15} \frac{9.7}{6} \frac{9.6}{14} \frac{9.8}{14} \frac{7.5}{15} \frac{14.5}{16}$



9.7 1154.41 ✓

1163 60

42 9.6 54.1

T.P. 9.96 1165 40 8.22 1155.14

43 7.8 57.6

44 4.0 61.4

45 6.6 58.8

B.M. 5.82 1159.58

+50 E. Cont. Box 6.6 58.8

Exc. Cond **CUINT**

3' x 2'

(No Work)

46 7.2 58.2

47 5.9 59.5

48 3.8 61.6

T.P. 10.71 1172 65 3.46 1161.94

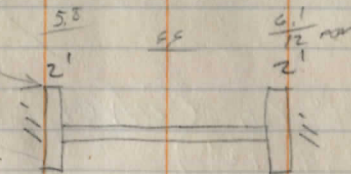
+2.7	+2.0	+0.1	0.0	-0.3	-0.7	+0.3
6.9	7.6	9.5	9.6	7.9	10.3	9.3
25	18	13		12	17	23-25

+4.6	+3.8	+0.4	-1.0	0.0	-0.4	+2.1
3.2	4.0	7.4	8.8	7.8	8.2	5.6
25	16	9	3		15	19-25

+3.2	+2.8	-0.7	-0.3	0.0	-0.5	-1.0	+1.3
0.8	1.2	4.7	4.3	4.0	4.5	5.0	2.7
25	15	9	5		13	18	21-25

+1.6	-0.8	-1.1	-0.3	0.0	-0.3	-1.6	-1.8
5.0	7.4	7.7	6.9	6.6	6.9	8.2	8.4
25	16	10	6		13	17	25

+ on parapet



+0.8	<12'	x	12'	7	-0.8	-0.6		
6.4	+0.1	-0.8	0.0	-0.4	-1.0	8.0	2.8	
25	7.1	8.0	7.2	7.6	8.2	12-15	16	25

-0.2	-0.7	-1.3	-0.4	0.0	-0.1	-1.1	-0.7	-1.3
6.1	6.6	7.2	6.3	5.9	6.0	7.0	6.6	7.2
25	15	14-12	10		9	14	15	25

+0.8	-0.2	-0.9	-0.5	0.0	-0.2	-0.8	+1.9	+3.8
3.5	4.0	4.7	4.3	3.8	4.0	4.6	1.9	0.0
25	13	11	10		8	10-13	18	25

1172⁷ 65

49 6.4 66.3

+75 4.0 68.7

50 4.3 68.4

51 5.1 67.6

52 6.5 66.2

+ 35 4 6" V.P. Culvert 6.2 66.5
(Reqd 12")

53 6.0 66.7

54 4.5 68.2

T.P. 391 1171 86 4.70 1167.95

+3.4	+1.7	+0.9	+0.7	-1.3	-0.8	0.0	-0.5	-1.1	+1.7	+2.2
3.4	1.7	0.9	0.7	1.3	0.8	0.0	0.5	1.1	1.7	2.2
25	4	19	15	11	10		10	14	19	25

+2.7	+1.1	-1.1	0.0	-0.9	+0.4	+0.7
2.7	1.1	1.1	0.0	0.9	0.4	0.7
25	14	11-9		15	17	25

+3.0	+1.3	-0.9	-0.3	0.0	-1.0	+0.8
3.0	1.3	0.9	0.3	0.0	1.0	0.8
25	3	10-8	6	4.3	5.3	21-25

-0.1	-1.2	-1.4	-0.4	0.0	-0.3	-1.5	-1.2	-2.5
0.1	1.2	1.4	0.4	0.0	0.3	1.5	1.2	2.5
25	11	10	5	5.1	5.4	6.6	6.3	7.6

+1.2	-0.5	-0.9	-0.1	0.0	-0.2	-0.9	-0.2	-0.1
1.2	0.5	0.9	0.1	0.0	0.2	0.9	0.2	0.1
25	19	10	7	6.5	6.7	7.4	6.7	6.6

-0.8	-1.1	-1.7	-1.9	-0.4	0.0	-0.6	-2.8	-3.2
0.8	1.1	1.7	1.9	0.4	0.0	0.6	2.8	3.2
25	15	13	10	8		9	12	25

< 10' x 12' >

+2.3	+0.7	-0.5	-1.1	0.0	-0.1	-0.9	+0.1
2.3	0.7	0.5	1.1	0.0	0.1	0.9	0.1
25	14	9	8	6.0	6.1	6.9	5.9

+1.8	+0.3	-0.7	0.0	-0.2	-1.2	-0.7	-0.8
1.8	0.3	0.7	0.0	0.2	1.2	0.7	0.8
2.5	12	10	4.5	4.7	5.7	5.2	5.3

✓

1171 8c

55

3.0 68.3

56

4.0 67.9

57

4.7 67.2

B.M.

1.89 1169.78

58

5.5 66.4

59

5.8 66.1

60

7.5 64.4

T.P.

2.47 1165 8 2

8.51 1169.35

61

2.0 63.2

62

3.2 62.6

63

4.9 60.9

$$\begin{array}{r} +1.9 \quad +0.8 \quad -0.8 \quad 0.0 \quad -0.2 \quad -0.7 \quad 0.0 \\ 1.7 \quad 2.3 \quad 4.4 \quad 3.4 \quad 3.8 \quad 4.3 \quad 3.0 \\ \hline 2.5 \quad 1.5 \quad 7 \quad \quad \quad 9 \quad 12 \quad 2.5 \end{array} \quad \checkmark$$

$$\begin{array}{r} +0.8 \quad +0.3 \quad -0.7 \quad 0.0 \quad -0.4 \\ 3.2 \quad 3.7 \quad 4.7 \quad 4.0 \quad 4.4 \\ \hline 2.5 \quad 1.7 \quad 1.4 \quad \quad \quad 1.3 \quad -2.5 \end{array} \quad \checkmark$$

$$\begin{array}{r} +1.5 \quad +1.0 \quad -1.0 \quad 0.0 \quad -0.7 \quad -0.2 \quad +0.6 \quad +0.7 \\ 3.2 \quad 3.7 \quad 5.7 \quad 4.7 \quad 5.4 \quad 4.7 \quad 4.1 \quad 4.0 \\ \hline 2.5 \quad 2.1 \quad 1.7-4 \quad \quad \quad 1.0 \quad 1.2 \quad 1.9 \quad 2.5 \end{array} \quad \checkmark$$

S.E. Root 15" Maple 25' Lt, Sta 57+10

$$\begin{array}{r} -0.3 \quad -0.8 \quad 0.0 \quad -0.4 \quad -1.0 \quad -1.8 \\ 5.8 \quad 6.3 \quad 5.3 \quad 5.9 \quad 6.5 \quad 7.3 \\ \hline 2.5 \quad 1.7-1.4 \quad \quad \quad 7 \quad 8-1.1 \quad 2.5 \end{array} \quad \checkmark$$

$$\begin{array}{r} +1.3 \quad +0.3 \quad -1.1 \quad -1.6 \quad -0.7 \quad 0.0 \quad -0.5 \quad -1.1 \quad -0.7 \quad +0.2 \\ 4.5 \quad 5.5 \quad 6.9 \quad 7.4 \quad 6.5 \quad 5.8 \quad 6.3 \quad 6.9 \quad 6.5 \quad 5.6 \\ \hline 2.5 \quad 2.0 \quad 1.7 \quad 1.4 \quad 1.1 \quad \quad \quad 9 \quad 1.2 \quad 1.3 \quad 2.5 \end{array} \quad \checkmark$$

$$\begin{array}{r} +0.8 \quad +0.1 \quad -1.0 \quad -1.3 \quad -0.8 \quad 0.0 \quad -0.5 \quad -1.1 \quad -0.1 \quad +0.2 \\ 6.7 \quad 7.4 \quad 8.5 \quad 8.8 \quad 8.5 \quad 7.5 \quad 8.0 \quad 8.6 \quad 7.6 \quad 7.3 \\ \hline 2.5 \quad 2.0 \quad 1.8 \quad 1.3 \quad 1.2 \quad \quad \quad 8 \quad 1.0 \quad 1.7 \quad 2.5 \end{array} \quad \checkmark$$

$$\begin{array}{r} -0.3 \quad -1.2 \quad -0.6 \quad 0.0 \quad -0.2 \quad -1.1 \quad -0.7 \\ 2.7 \quad 3.8 \quad 3.2 \quad 2.6 \quad 2.8 \quad 3.7 \quad 3.3 \\ \hline 2.5-1.9 \quad 1.4 \quad 1.1 \quad \quad \quad 7 \quad 9 \quad 2.5 \end{array} \quad \checkmark$$

$$\begin{array}{r} +0.1 \quad -0.3 \quad -0.8 \quad -1.4 \quad -0.8 \quad 0.0 \quad -0.3 \quad -0.9 \quad -0.2 \quad -0.1 \\ 3.1 \quad 3.5 \quad 4.0 \quad 4.6 \quad 4.0 \quad 3.2 \quad 3.5 \quad 4.1 \quad 3.4 \quad 3.3 \\ \hline 2.5 \quad 1.9 \quad 1.7 \quad 1.3 \quad 1.2 \quad \quad \quad 7 \quad 1.0 \quad 1.5 \quad 2.5 \end{array} \quad \checkmark$$

$$\begin{array}{r} 0.0 \quad -1.8 \quad -0.7 \quad 0.0 \quad -0.7 \quad 0.0 \quad +1.5 \\ 4.9 \quad 6.7 \quad 5.6 \quad 4.4 \quad 5.6 \quad 4.9 \quad 7.5 \\ \hline 2.5-2.0 \quad 1.6 \quad 1.3 \quad 1.1 \quad 1.4 \quad 1.0 \quad 1.5 \end{array} \quad \checkmark$$

116582

64 7.0 58.8

6.5 10.2 55.6
T.P 1.46 115624 11.04 1154.78

66 4.2 52.0

67 7.4 48.8

+50 4 12" C.I.P. sec) 8.2 48.0
(Reg'd 12") Culvert
outlet

68 8.2 48.0

B.M. 2.89 1153.35

69 5.5 50.7
T.P. 1.73 1152.21 5.76 1150.48

70 6.9 45.4

13

+1.5	+0.9	-1.1	-1.7	-0.8	0.0	-0.5	-1.6	+1.2	+2.4	✓
5.5	6.1	8.1	8.7	7.8	7.0	7.5	8.6	5.8	4.6	
25	20	17	15	14		4	7	14	25	

+1.9	+1.2	-0.5	-1.4	-0.5	0.0	-0.3	-1.5	-0.4	+0.8	+1.7
8.3	9.0	10.7	11.6	10.7	10.2	10.5	11.7	10.6	7.7	8.3
25	20	19	17	12		3	6	10	18	25

+3.9	+2.5	-1.0	-1.5	-0.3	0.0	-0.4	-0.8	-0.3	+1.3	+2.1
0.3	1.7	5.2	5.7	4.5	4.2	4.6	5.0	4.5	2.9	2.1
25	20	16	14	13	11		5	10	13	25

LT bank ends 1150

-0.5	-0.2	-0.9	-0.4	0.0	-0.3	-0.9	+0.1	-1.0		
7.9	7.6	8.3	7.8	7.7	7.7	8.3	7.3	8.4		✓
25	15	12	11		3	4	7	9	25	

-1.1	-1.6	-0.3	0.0	-0.2	-2.2	-1.9	-3.4			
9.3	8.8	8.5	8.2	8.4	10.4	10.1	11.6			
25	13	11		5	7	25	50			

< 13 x 7 > 10

+1.2	+0.1	-1.1	-0.3	0.0	-0.2	-1.0	+0.1	-0.5		
7.0	8.1	9.3	8.5	8.7	8.4	9.2	8.1	8.7		✓
25	21	13	11		5	17	22	25		

E. root 20" Maple 25' Lt, sta. 68+30

0.0	-1.1	-1.3	-0.7	0.0	-0.1	+1.9	+2.3			
5.5	6.6	6.8	6.2	5.5	5.6	3.6	3.2			✓
18-25	15	13	11		8	16	25			

+2.4	+1.2	-1.2	-0.3	0.0	-0.3	-0.9	+2.7	+3.2		
11	5.6	8.0	7.1	6.8	7.1	7.7	3.9	3.6		✓
25	16	13	10		2	3	12	25		

1152 21

TP 4.90 1144 71 12.40 1139.81
 71 7.3 37.4

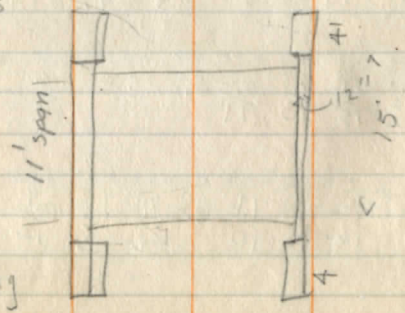
+50 9.5 35.2

+90 10.8 33.9

72 10.7 34.0

S.P. 6.06 1142 52 8.25 1136.75
 bottom of slab 8.07 ~~36.61~~
 top " " 7.13 ~~37.58~~

+32 & span. Con. slab. Bridge
 stone Abuts. Con. Slab & Comb.
 Fair Cond.
 Point-Abuts $\times 10.6' \times 7.4'7$



4 1/2 ft. opening

+2.7	0.0	-0.9	-0.4	0.0	-0.4	-1.2	+3.1	+4.7	✓
<u>4.6</u>	<u>7.3</u>	<u>8.2</u>	<u>7.7</u>	<u>7.3</u>	<u>7.7</u>	<u>8.5</u>	<u>4.2</u>	<u>2.6</u>	
25	17-15	13	10		4	2-8	14	21-25	

+1.2	-0.5	-0.8	-0.5	0.0	-0.4	-0.8	0.0	
<u>8.3</u>	<u>10.0</u>	<u>10.3</u>	<u>10.0</u>	<u>9.5</u>	<u>9.9</u>	<u>10.3</u>	<u>9.5</u>	
25	19	13	10		6	8	12-25	

-0.8	-1.5	-2.1	-2.5	-0.6	0.0	-0.5	0.0	-0.6
<u>11.6</u>	<u>13.1</u>	<u>12.7</u>	<u>13.3</u>	<u>11.4</u>	<u>10.8</u>	<u>11.3</u>	<u>10.8</u>	<u>11.4</u>
25	17	16	8	4		11	12	25

-1.5	-2.5	-0.2	0.0	+0.2	-0.6	0.0	-0.5
<u>12.7</u>	<u>13.7</u>	<u>10.9</u>	<u>10.7</u>	<u>10.5</u>	<u>11.3</u>	<u>10.7</u>	<u>11.2</u>
25	20-12	9		10	13	14	25

~~4.0~~ x S.W. cor w. parapet -
 34.4
 35.4

1142 52

724

7.3 35.2

+40

7.2 35.3

73

8.7 33.8

E Rt +20

7.9 34.6

28' Lin. ft. 10" cor pipe
under Rd. to Lt. E. ditch
drains down N. ditch of
Rd. to East.

8.6 33.9

11.0 31.5

8.1 34.4

5.8 36.7

74

Rt.

5.9 36.6

T.P. 10.07 1149.98

2.61 1139.98

+30

11.7 38.3

75

6.9 43.1

T.P. 11.04 1159.33

1.69 1148.29

76

8.2 51.1

+65

6.6 53.8

Killed 3 snakes 3-17-21

15

$$\begin{array}{r} -4.2 -1.3 +0.5 \quad 0.0 \quad 0.0 \quad +0.6 \quad -1.0 \quad -1.8 \quad -2.4 \quad -2.2 \\ 11.5 \quad 8.6 \quad 6.8 \quad 7.3 \quad 7.3 \quad 6.7 \quad 8.3 \quad 9.1 \quad 9.7 \quad 9.5 \\ 25-19 \quad 12 \quad 11 \quad 10.9 \quad \quad \quad 6 \quad 7 \quad 15 \quad 14 \quad 25 \end{array}$$

$$\begin{array}{r} -4.1 -3.7 -1.8 \quad +0.1 \quad 0.0 \quad +0.5 \quad -2.1 \quad -0.6 \quad -2.4 \\ 11.3 \quad 10.9 \quad 9.0 \quad 7.1 \quad 7.2 \quad 6.7 \quad 9.3 \quad 9.2 \quad 9.6 \\ 25 \quad 20 \quad 12 \quad 10.9 \quad \quad \quad 5.6 \quad 7 \quad 12 \quad 25 \end{array}$$

$$\begin{array}{r} -0.4 -1.5 -0.2 -0.6 \quad 0.0 \quad -1.1 \quad -1.6 \quad \checkmark \\ 3.1 \quad 10.2 \quad 8.1 \quad 9.3 \quad 8.7 \quad 9.8 \quad 10.3 \\ 25-18 \quad 15 \quad 14-11 \quad 9 \quad \quad \quad 14 \quad 25 \end{array}$$

10' Rt.

100' Rt

20' Lt

100' Lt.

$$\begin{array}{r} +1.0 -0.3 -0.7 -1.3 -0.4 \quad 0.0 \quad -0.2 -0.6 +0.3 +1.4 +2.5 +4.9 \\ 4.9 \quad 6.2 \quad 6.6 \quad 7.2 \quad 6.3 \quad 5.9 \quad 6.1 \quad 6.5 \quad 5.6 \quad 4.5 \quad 3.4 \quad 1.0 \\ 25 \quad 21 \quad 14 \quad 15 \quad 12 \quad \quad \quad 7 \quad 10 \quad 14 \quad 16 \quad 20 \quad 25 \end{array}$$

$$\begin{array}{r} +2.6 +2.3 -1.0 -0.5 \quad 0.0 \quad -0.2 +5.5 +7.6 \\ 9.1 \quad 9.4 \quad 12.7 \quad 12.2 \quad 11.7 \quad 11.7 \quad 6.3 \quad 9.1 \\ 25 \quad 20 \quad 12 \quad 11 \quad \quad \quad 10 \quad 18 \quad 25 \end{array}$$

$$\begin{array}{r} +5.7 +4.7 -0.1 \quad 0.0 \quad +0.1 -0.5 +5.2 +6.3 \\ 1.2 \quad 2.2 \quad 7.0 \quad 6.9 \quad 6.3 \quad 7.4 \quad 1.7 \quad 0.6 \\ 25-23 \quad 20 \quad 14 \quad \quad \quad 5 \quad 6 \quad 14 \quad 25 \end{array}$$

(Deduct 10 cu. yds. for drive to Rt.)

$$\begin{array}{r} +5.2 +4.5 -1.2 -0.4 \quad 0.0 \quad -0.7 +3.9 +4.7 \\ 30 \quad 3.7 \quad 9.1 \quad 8.6 \quad 8.2 \quad 8.9 \quad 4.3 \quad 3.5 \\ 25 \quad 20 \quad 17 \quad 9 \quad \quad \quad 8 \quad 15 \quad 25 \end{array}$$

$$\begin{array}{r} +6.0 +5.5 +3.1 -0.5 \quad 0.0 \quad -0.5 +3.3 +2.9 \\ -0.5 \quad 0.1 \quad 2.4 \quad 6.0 \quad 6.5 \quad 6.0 \quad 2.5 \quad 2.9 \\ 25 \quad 20 \quad 13 \quad 19 \quad \quad \quad 10 \quad 15 \quad 25 \end{array}$$

(Deduct 5 cu. yds. for old drive Rt.)

1159 33

77 44 54.9

+4.4	+3.5	-0.3	0.0	-0.3	-0.9	+1.0	+0.9	✓
<u>0.0</u>	<u>0.9</u>	<u>4.7</u>	<u>4.4</u>	<u>4.7</u>	<u>5.3</u>	<u>3.1</u>	<u>3.5</u>	
<u>2.5</u>	<u>1.5</u>	<u>1.0</u>		<u>1.0</u>	<u>1.2</u>	<u>1.6</u>	<u>2.5</u>	

~~+3078~~ 3.8 55.5

+2.0	+0.7	-0.7	0.0	-0.5	-1.3	-0.2	+0.1	-0.2
<u>1.8</u>	<u>2.9</u>	<u>4.5</u>	<u>3.8</u>	<u>4.3</u>	<u>5.1</u>	<u>4.0</u>	<u>3.7</u>	<u>4.0</u>
<u>2.5</u>	<u>1.5</u>	<u>1.0</u>		<u>9</u>	<u>12</u>	<u>17</u>	<u>2.0</u>	<u>2.5</u>

78 4.9 54.4

+0.6	+0.5	-0.9	0.0	-0.9	-0.5	-0.7	✓
<u>4.3</u>	<u>4.4</u>	<u>5.3</u>	<u>7.9</u>	<u>5.8</u>	<u>5.4</u>	<u>5.6</u>	
<u>2.5</u>	<u>1.3</u>	<u>1.0</u>		<u>1.3</u>	<u>1.4</u>	<u>2.5</u>	

79 8.2 51.1

+2.2	-0.3	-0.6	-1.6	-0.6	0.0	-0.4	-1.1	+2.1	+2.7	✓
<u>2.0</u>	<u>3.5</u>	<u>8.9</u>	<u>9.8</u>	<u>8.8</u>	<u>8.2</u>	<u>8.9</u>	<u>9.3</u>	<u>6.1</u>	<u>5.5</u>	
<u>2.5</u>	<u>1.9</u>	<u>1.5</u>	<u>1.2</u>	<u>1.1</u>	<u>1.8</u>	<u>9</u>	<u>12</u>	<u>1.8</u>	<u>2.5</u>	

~~+70~~ 10.5 48.8

+1.0	-0.5	-1.1	-0.3	0.0	-0.1	-0.8	+1.0	+1.2	
<u>9.5</u>	<u>11.0</u>	<u>11.6</u>	<u>10.3</u>	<u>10.5</u>	<u>10.6</u>	<u>11.3</u>	<u>9.5</u>	<u>9.3</u>	
<u>2.5</u>	<u>1.8</u>	<u>1.3</u>	<u>1.2</u>	<u>9</u>	<u>8</u>	<u>11</u>	<u>14</u>	<u>1.8</u>	<u>2.5</u>

80 11.2 48.1

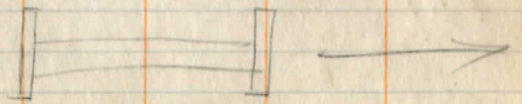
-0.1	+0.1	-0.2	-0.8	0.0	-0.3	-0.7	-0.4	-1.3	✓
<u>11.3</u>	<u>11.1</u>	<u>11.4</u>	<u>12.0</u>	<u>11.2</u>	<u>11.5</u>	<u>11.9</u>	<u>11.6</u>	<u>12.5</u>	
<u>2.5</u>	<u>1.7</u>	<u>1.3</u>	<u>1.2</u>		<u>8</u>	<u>11</u>	<u>14</u>	<u>2.5</u>	

T.P. 7.78 1157 85 9.25 1150.07 x art Lt. Head Wall. Culv.

+73 & stone culvert 9.3 48.6

con. cover,
3 x 3
good cond
O.K.

Length:



<12'-6" x 12'-0">

1157.85

81 9.3 48.6

82 8.6 49.3

+2.5 7.4 50.5

83
T.P. 10.86 1167 61 5.1 52.8
1.10 1156.75

84 9.0 58.6

85 4.8 62.8

86
T.P. 9.28 1175 71 1.7 65.9
1.18 1166.43

87 8.0 67.7

88 8.3 69.5

B.M. 199 1173.72

17
✓

-1.5 -0.6 -1.0 -0.2 0.0 -0.4 -1.4 -0.8 -2.1
108 97 103 95 93 97 107 101 114
25 13 12 11 9 12 13 25

-0.4 -0.7 0.0 -0.1 -0.7 -0.2 +1.0 +1.6
9.0 9.3 8.6 8.7 9.3 8.8 7.6 7.0
25 9 8 10 11-14 18 25

+2.0 -0.9 -1.6 -0.4 0.0 -0.6 -1.3 -0.9 +1.3 +2.0
5.4 8.3 9.0 7.8 7.4 8.0 8.7 8.3 6.1 5.4
25 15 9 2 1 8 10 12 15 25

+5.9 +4.9 -0.5 -1.1 0.0 0.0 -0.5 +3.6 +4.4
-0.8 0.2 5.6 6.2 5.1 5.1 5.6 1.5 1.2 ✓
25-22 20 11-10 9 8 8-11 17 25

+5.7 +5.1 -0.6 -1.2 -0.4 0.0 -0.2 -1.0 +0.6 +2.6 ✓
3.3 3.9 9.6 10.2 9.4 9.0 9.2 10.0 9.6 6.9
25 20 11.9 8 2 10 12 14 19-25

+2.1 +0.7 -1.0 0.0 0.0 -0.4 -0.7 +0.5 ✓
2.7 4.1 5.3 4.8 4.8 5.2 5.7 4.3
25 14 11 9 10 12 15-25

-0.1 -0.5 -1.6 -0.5 0.0 -0.3 -1.2 -0.7 -0.5
1.8 2.2 3.3 2.2 1.7 2.0 2.9 2.4 2.2 ✓
25 16 14 13 11 12 13 25

+0.4 +0.3 -1.3 0.0 -0.5 -1.4 -1.0 +1.7
7.6 7.7 9.3 8.0 8.5 9.4 9.0 6.3 ✓
25 20 14 9 10 15-18 25

+2.1 -1.2 0.0 -0.3 -0.7 +2.1 ✓
4.1 7.4 6.7 6.5 6.7 4.1
25-21 13 11 15 23-25

B.M. 978 118350 1173.72

89 10.7 72.8

90 7.7 75.8

91 5.1 78.4

+50 4.3 79.2

92 5.7 78.1

93 8.0 75.5

+73 7.9 75.6

£ stone box
A x 2? Culvert
clean cut outlet 100'
clean Culv. 1' mud from bottom
Ext. Good cond

94 7.5 76.0

95 5.4 78.1

+1.9 +2.4 -0.7 0.0 -0.3 -0.9 +0.6 +1.8
 $\frac{5.8}{25} \frac{8.3}{19} \frac{11.4}{11} \frac{10.7}{11} \frac{11.0}{13} \frac{11.6}{15} \frac{10.1}{18} \frac{8.9}{25}$

+2.5 -1.0 -0.2 0.0 -0.6 +0.3 +0.1
 $\frac{5.2}{25} \frac{8.7}{19} \frac{7.9}{8} \frac{7.7}{8} \frac{8.3}{14} \frac{7.4}{16} \frac{7.6}{25}$

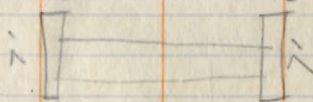
+2.0 -0.3 0.0 -0.6 -0.9 -0.5 -0.4
 $\frac{3.1}{25} \frac{5.9}{20} \frac{5.1}{11} \frac{5.7}{12} \frac{6.0}{14} \frac{5.6}{15} \frac{5.5}{25}$

+0.3 -0.1 -0.7 -0.4 0.0 -0.3 -1.2 -0.9 -0.2
 $\frac{4.0}{25} \frac{4.4}{15} \frac{5.0}{14} \frac{4.7}{10} \frac{4.3}{10} \frac{4.6}{10} \frac{5.5}{14} \frac{5.2}{15} \frac{4.5}{25}$

+0.4 +0.1 -1.4 -0.4 0.0 -0.3 -1.3 +0.4 +1.7
 $\frac{5.0}{25} \frac{5.3}{15} \frac{6.2}{11} \frac{5.8}{8} \frac{5.9}{8} \frac{5.7}{10} \frac{6.7}{14} \frac{5.9}{20} \frac{3.7}{25}$

-0.6 -0.2 0.0 -0.4 -1.1 +0.1 +1.2
 $\frac{8.4}{25} \frac{8.2}{11} \frac{8.0}{10} \frac{8.4}{10} \frac{8.1}{12} \frac{7.9}{21} \frac{6.8}{25}$

+3.2 -3.4 -0.3 0.0 +0.1 -3.5 -3.6
 $\frac{11.0}{25} \frac{11.3}{10} \frac{8.2}{9} \frac{7.9}{9} \frac{7.8}{10} \frac{11.7}{15} \frac{11.5}{25}$



< 10'-6" x 10' >

-2.1 -0.8 0.0 -0.3 -2.3
 $\frac{9.6}{25} \frac{8.3}{12} \frac{7.5}{14} \frac{7.8}{14} \frac{9.8}{25}$

+1.6 -0.8 -0.6 -0.9 -0.3 0.0 -0.3 -1.0 -0.6 -0.4 +1.6
 $\frac{3.8}{25} \frac{6.2}{19} \frac{6.0}{11} \frac{6.3}{10} \frac{5.7}{8} \frac{5.1}{8} \frac{5.7}{8} \frac{6.4}{11} \frac{6.0}{12} \frac{5.6}{20} \frac{3.9}{25}$

123031

T.P. 12.53 1240 80 ✓ 2.04 1228.27 ✓

104 9.8 31.0

105 5.6 35.2

+ 98 £ 10" C.I.P. Culvert
Road 12" hillside

106 ✓ 1.4 39.4 ✓

T.P. 10.71 1250 29 1.22 1239.58

107 8.5 41.8

108 ✓ 6.0 44.3 ✓

T.P. 12.45 1259 74 3.00 1247.24

109 11.4 48.3

110 6.0 53.7

20

+2.0	+0.1	-0.9	-0.3	0.0	-0.3	-0.8	+1.2
7.8	9.7	10.7	10.1	9.8	10.1	10.6	8.6 ✓
25-17	14	11	9	rock	11	14	12.25
+3.4	-0.4	-0.6	0.0	-0.4	-1.0	+0.3	+2.5 ✓
2.2	0.0	6.2	5.6	6.0	4.6	5.3	3.1
25-19	14	9	rock	11	13	17	22-25

+0.7	-1.2	+0.5	0.0	0.0	-0.4	-1.6	-2.1
0.7	2.6	0.9	1.4	1.4	1.3	3.0	3.5
25-15	14.1	9.7	1.4	1.4	1.3	2.1	2.5

diskon

5' x 13'

+0.3	-1.5	+0.2	-0.4	0.0	-0.3	-0.4	+0.1	-0.2	-0.6
0.3	2.6	0.9	1.5	1.1	1.4	1.5	1.0	1.3	1.2 ✓
25-15	11	8	6	11	11	14	15	13	1.2
0.0	-0.5	-0.8	-0.2	0.0	-0.3	-0.9	-0.1	+0.5	
2.5	9.0	9.3	8.7	8.5	8.8	9.4	8.6	8.0	
25-20	11	10	17	12	14	16	30		
+2.0	+1.5	0.0	0.0	-0.3	+1.3				
2.0	1.5	6.0	6.0	6.3	1.3				
25	17	12	6.0	1.4	2.5				

+4.4	+2.0	-0.9	+0.4	0.0	+0.2	-0.8	-0.2	+3.7	+4.1
7.0	9.4	12.3	11.5	11.9	11.2	12.2	11.6	7.7	7.3
25-18	11-12	8	6	10	12	14	19	25	
+2.7	+2.4	+1.5	-1.1	-0.2	0.0	-0.4	-0.8	+1.6	
2.7	2.4	1.5	7.1	6.2	6.0	6.4	6.8	4.4	
25	17	13	7.6	4	11	13	19-25		

111

2.3 57.4

B.M.

T.F. 5.33 12.64 37

112

4.6 59.8

+50

4.1 60.3

113

5.7 59.0

114 2 & 2 Stone Box
3' x 2 1/2' Culvert
Good Cond. OK

5.8 58.6

T.P. Temp B.M. E. Poropot.

5.17 1259.20

115

5.0 59.4

+85

2.2 62.2

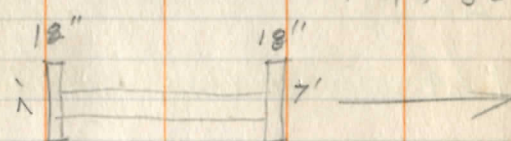
116

2.3 62.1

+1.5 +0.3 -0.5 0.0 -0.5 +0.4
 $\frac{9.8}{2.5} \frac{2.0}{12} \frac{2.8}{11} \frac{2.3}{12} \frac{2.8}{12} \frac{1.9}{20-25}$

Nails W root 60" Elm 35' Rt, Sta 110+25

+1.4 -0.2 -1.0 0.0 -0.3 -0.9 +0.4
 $\frac{3.2}{25-23} \frac{4.8}{10} \frac{5.6}{7} \frac{4.6}{13} \frac{4.9}{15} \frac{5.5}{19-25} \frac{4.2}{19-25}$
 +2.4 +1.3 -1.0 -0.4 0.0 -0.6 -0.5
 $\frac{1.7}{2.5} \frac{2.8}{14} \frac{5.1}{10} \frac{4.5}{7} \frac{4.1}{7} \frac{4.7}{16} \frac{4.6}{25}$
 +3.6 +1.1 +0.8 -1.4 -0.5 0.0 -1.2 +0.1 +0.2
 $\frac{1.8}{2.5} \frac{4.3}{18} \frac{4.6}{16} \frac{6.3}{14} \frac{5.9}{11} \frac{5.7}{8} \frac{6.0}{15-17} \frac{5.8}{19} \frac{5.6}{25}$
 -3.4 -3.8 +0.8 -0.2 0.0 +0.1 +0.6 -3.5 -4.0
 $\frac{9.2}{2.5} \frac{9.6}{Fl.} \frac{5.0}{Par.} \frac{6.0}{14} \frac{5.8}{14} \frac{5.7}{12} \frac{5.2}{Par.} \frac{9.3}{Fl.} \frac{9.8}{30}$



< 10' x 14' >

+3.0 +1.0 -1.1 -1.6 -0.9 0.0 -0.4 -1.5 -0.6 +0.4 +0.5
 $\frac{2.0}{2.5-23} \frac{4.0}{21} \frac{6.1}{17} \frac{6.6}{12} \frac{5.9}{10} \frac{5.0}{14} \frac{5.4}{14} \frac{6.5}{16} \frac{5.6}{17} \frac{4.6}{21} \frac{4.5}{25}$
 +1.9 +0.9 +0.2 0.0 -0.2 -0.0
 $\frac{0.3}{2.5-21} \frac{1.3}{19} \frac{2.0}{6} \frac{2.2}{14} \frac{2.7}{14} \frac{2.7}{25}$
 +2.1 +1.4 +1.1 +0.2 -0.2 0.0 -0.4 -0.3
 $\frac{0.7}{2.5-22} \frac{0.7}{2.0} \frac{1.2}{1.5} \frac{2.1}{13} \frac{2.5}{10} \frac{2.3}{18} \frac{2.7}{18} \frac{2.6}{2.5}$

117		2.3	62.1
T.P.	0.79	1264	31 ✓
118		2.5	61.8
119		5.5	58.8
120		8.1	56.2
121		8.9	55.4
122		9.0	54.7
+24	END of Cor.	10.3	54.0
B.M.		4.75	1259.56 ✓
+50		9.4	54.9
123		10.0	54.3
124		11.5	49.8
T.P.	25 ⁰	1255	49 ✓
		11.22	1253.09 ✓

+0.6	-0.6	1.1	-0.5	0.0	-0.3	-1.5	
1.7	2.5	3.9	2.8	2.3	2.6	3.8	✓
2.5	1.4	12-10	9	14	22-25		
+1.4	+0.6	-1.3	-0.4	0.0	-0.3	-1.2	-1.6
1.1	1.9	3.8	2.9	2.5	2.8	3.7	4.1 ✓
2.5-23	14	12-11	7	8	18	25	
+3.2	+1.7	+0.1	0.0	-0.3	+0.7	+1.1	✓
2.9	3.8	5.4	5.5	5.3	4.8	4.4	
15-13	-12	16-19	21	25			
+1.2	-0.5	-0.9	-0.1	0.0	-1.0	-0.7	-0.3
6.9	8.4	9.0	8.2	8.1	9.1	8.8	8.4 ✓
2.6	22-18	17	10	16	17	25	
-0.7	-1.1	-1.2	0.0	-0.3	-1.3	-0.9	✓
9.6	10.0	9.1	8.9	9.2	10.2	9.8	
2.6	15	12	15	19	25		
-0.3	-1.6	-0.3	+0.2	0.0	-0.6	-1.4	✓
9.9	11.2	9.7	9.4	9.6	10.2	11.0	
2.4	2.3	22-18	15	11-17	25		
+0.5			0.0				
8.9	9.4	10.5	2.5				
+1.4	+0.6		0.0				
8.4	9.3	10.0	10.0	10.0	10.0	10.0 ✓	
2.5	2.1	16	25				
+2.0	+0.3		0.0				
13.5	14.2	14.5	14.6	15.6	14.7 ✓		
2.5	14	12	18	25			

X on S.W. Cor. Cor. Porch to Store.

1255 47

125

6.4 49.1

+0.8

stone Box Culvert
Good cond

1249.1

126

6.0 49.5

127

3.9 51.6

128

3.5 52.0

129

4.3 51.2

130

4.8 50.7

131

4.5 51.0

132

✓ 5.8 49.7

T.P.

1.72 1250 41

6.80 1248.69

133

6.5 43.9

134

4.8 40.5

9.9

23

6.4

$$\begin{array}{r} -1.2 \quad -0.6 \quad 0.0 \quad 0.0 \quad -1.0 \quad -3.6 \\ 7.5 \quad 7.0 \quad 6.4 \quad 6.9 \quad 7.7 \quad 10.0 \\ \hline 44.9 \quad 10.5 \quad 7.0 \quad 6.4 \quad 7.3 \quad 11.5 \\ \hline 2 \quad 12 \quad 18 \end{array}$$

13th T/He

$$\begin{array}{r} +1.6 \quad +1.1 \quad -0.2 \quad 0.0 \quad -0.6 \quad -1.5 \quad +0.8 \quad 0.0 \\ 4.4 \quad 4.9 \quad 6.2 \quad 6.0 \quad 6.6 \quad 7.5 \quad 6.8 \quad 6.0 \\ \hline 24 \quad 16 \quad 9 \quad 6.0 \quad 14 \quad 16-19 \quad 20 \quad 25 \\ \hline +0.1 \quad -1.3 \quad -0.4 \quad 0.0 \quad -0.5 \quad -1.0 \quad -0.6 \\ 3.8 \quad 5.2 \quad 4.3 \quad 3.9 \quad 4.4 \quad 5.5 \quad 4.5 \\ \hline 25-20 \quad 11 \quad 9 \quad 15 \quad 17 \quad 18 \quad 5 \\ \hline +3.1 \quad +1.4 \quad -0.3 \quad -1.2 \quad -0.4 \quad 0.0 \quad -0.3 \quad -1.0 \quad -0.6 \quad -0.1 \\ 0.7 \quad 2.1 \quad 3.8 \quad 4.7 \quad 3.9 \quad 3.8 \quad 3.7 \quad 4.5 \quad 4.1 \quad 3.6 \\ \hline 25 \quad 7C \quad 15-13 \quad 12 \quad 8 \quad 14 \quad 18 \quad 19 \quad 25 \end{array}$$

$$\begin{array}{r} +1.8 \quad +1.4 \quad -0.6 \quad 0.0 \quad -0.5 \quad -1.5 \quad -0.7 \quad -0.5 \\ 2.5 \quad 2.9 \quad 4.7 \quad 4.3 \quad 4.8 \quad 5.8 \quad 5.0 \quad 4.8 \\ \hline 25 \quad 19 \quad 13 \quad 13 \quad 15 \quad 19 \quad 20 \quad 25 \\ \hline +1.0 \quad +0.1 \quad -1.0 \quad -0.3 \quad 0.0 \quad -0.5 \quad -1.6 \quad -0.6 \quad -1.6 \\ 3.8 \quad 4.7 \quad 5.8 \quad 5.1 \quad 4.8 \quad 5.3 \quad 6.4 \quad 5.8 \quad 6.4 \\ \hline 25 \quad 15 \quad 13-9 \quad 8 \quad 14 \quad 17 \quad 18 \quad 25 \end{array}$$

$$\begin{array}{r} +2.8 \quad +1.8 \quad -2.3 \quad -0.2 \quad 0.0 \quad -0.2 \quad -1.4 \quad +0.1 \quad +1.4 \\ 1.7 \quad 2.7 \quad 3.8 \quad 4.7 \quad 4.5 \quad 4.7 \quad 5.9 \quad 4.4 \quad 3.1 \\ \hline 25 \quad 21 \quad 14 \quad 17 \quad 17 \quad 14 \quad 17 \quad 20 \quad 25 \end{array}$$

$$\begin{array}{r} +3.7 \quad -2.2 \quad 0.8 \quad 0.0 \quad -0.3 \quad -1.2 \quad -0.3 \quad +3.8 \\ 2.1 \quad 3.0 \quad 6.6 \quad 5.8 \quad 6.1 \quad 7.0 \quad 6.1 \quad 2.0 \\ \hline 25 \quad 15 \quad 14 \quad 11 \quad 11 \quad 14 \quad 16 \quad 25 \end{array}$$

$$\begin{array}{r} +3.0 \quad +0.4 \quad -0.5 \quad -1.3 \quad -0.2 \quad 0.0 \quad -0.2 \quad -1.2 \quad -0.5 \quad +3.8 \\ 3.5 \quad 6.1 \quad 7.0 \quad 7.8 \quad 6.7 \quad 6.5 \quad 6.7 \quad 7.7 \quad 7.0 \quad 3.8 \\ \hline 25 \quad 19 \quad 16 \quad 15 \quad 12 \quad 10 \quad 10 \quad 12 \quad 15 \quad 20 \quad 25 \\ \hline -2.0 \quad -1.6 \quad -0.7 \quad 0.0 \quad -0.1 \quad -1.1 \quad -2.0 \\ 11.7 \quad 11.5 \quad 10.6 \quad 9.9 \quad 10.0 \quad 11.0 \quad 11.9 \\ \hline 25 \quad 17 \quad 15 \quad 11 \quad 14 \quad 25 \end{array}$$

1250 41

Culvert

134+43 4 Stone Box 100 40.4

2x3 Box Con floor

Temp B.M.

O.K.

9.08 1241.33 ✓

135

10.8 39.6

136

7.7 42.5

137

5.1 45.0

+69' End of Survey.

8.4 42.0

15.5 34.9

24

35.3								
-5.1	+0.9	-0.1	0.0	+0.6				-5.9
15.1	9.1	10.1	10.0	9.2				15.9
FL	15	13.0		14				FL

< 15 x 15 >

+0.9	+0.4	-0.7	-1.0	-0.3	0.0															
32	12.4	11.5	11.8	11.1	10.8															
30	21	19	13	12																
+4.5	+3.8	+1.8	-1.0	-0.1	0.0															
34	41	41	39	38																
25	20	16	11.9	8																
+3.9	+2.9	-0.7	-0.3	0.0																
15	25	6.1	5.7	5.4																
25	17	12-10	9																	
+3.5	+2.8	-0.3	0.0																	
19	5.6	8.7	8.9																	
25	16	12																		

100' N. of end

			1259.56
			1249.99
0.17	1259.73		1259.56
1.36	1253.90	8.19	1251.54
3.81	1247.98	7.73	1244.17
0.25	1246.08	2.13	1245.83
1.85	1236.27	11.16	1234.92
5.18	1241.18	0.27	1236.00
		0.54	1240.64
0.93	1229.13	12.98	1228.30
2.52	1229.27	2.38	1226.75
4.85	1233.42	0.70	1228.57
		5.32	1228.10
4.54	1234.06	3.90	1229.52
3.26	1225.68	11.64	1222.42
		2.71	1222.97
7.49	1231.23	6.94	1223.74
5.15	1236.18	0.20	1221.13
		1.27	1234.91
3.50	1234.09	5.57	1230.57
3.17	1240.62	1.64	1232.45
		2.00	1238.62
3.48	1243.72	0.38	1240.24
6.96	1249.58	1.00	1242.72
		3.16	1246.53
3.98	1253.13	0.53	1247.15

Oct 31, 1923 Marks
Snow Flurries Thompson

25

x on S.W. Cor. Porch to store, (N.W. ^{crossroad} Cor. of)
x on W. parapet, Culvert 100' N. of ^{Huntsburg} ~~Montville~~ ^{Montville} Trp. line.

Spike, S.W. Root Maple, R. 139+6911
Spike, N.W. " " R. 147+65

Ref. Nat, E. side Trunk 36" Elm, R. 164+25

Spike, W. Root 15" Evergreen, R. 173+05 ✓
" " " 16" Cedar, ^(N. Trunk in Cove) R. 187+80
Spike, W. Root 18" Cedar, R. 187+80.

Spike, N.W. Roots Maple R. 202+20

Spike, N.E. Root 20" Maple L. 216+35
Bent Spike, E. Root 24" Maple, L. 224+30 ^{J. Whites House}
Spike L. 228+75
Spike E. root 30" Elm L. 238+75

Spike E. root 10" Maple
Spike, E. root 10" Maple L. 250+05

1258.13

0.22 1257.91

8.47 1249.66

Spice, E, Root 30" Maple, L. 255 x 60
 x, N.W. Cor. W. H. W., 100' N. of Twp. L. in e
 1249.99 as run from Montvill Center

Sta. B.S. H.I. F.S. Elev.

B.M. 140 1245.57 1244.17
138 5.8 1239.8

+60 10.1 1235.5

139 13.6 1232.0

0.83 1233.65 12.75 1232.82

140 4.9 1228.8

+28 4.8 1228.9

+38 Good Condition 2' wide at W. End 1229.6
Stenc. Box good 2 1/2" " E. " 1224.2

+48 5.5 1228.2

141 5.3 1228.4

142+50 3.9 1229.8

12.30 1245.95 0.00 1233.65

143 12.6 1233.4

+50 7.7 1238.3

143 4.7 1241.3

+70 2.0 1244.0

Nov. 1, 1923
Fair-Cool

Marks } chicken Dinner at 27
Grad } 1 day, Culbertson's.
Thompson } \$1.50, Marks
2 1/2" photo, \$2.70 "

R. 137 +69.11
+4.6 +2.9 -0.5 -0.2 0.0 -0.3 -0.7 -0.5 +1.1 +1.4 +1.3
1.2 2.4 6.3 6.0 5.8 6.1 5.5 6.3 4.2 4.4 4.5
30 16 11 8 5.8 9 13 14 18.5 27 30

+6.0 +4.2 -0.4 -0.5 -0.1 0.0 -0.3 -0.6 -0.2 +4.8 +4.5
4.2 5.7 10.5 10.6 10.2 10.1 10.4 10.7 10.3 5.3 5.6
30 14.8 16.5 9 8 8 8 11 17 28

+3.2 +2.7 -0.5 -0.2 0.0 -0.3 -1.0 +2.7 +3.7 +5.0 +5.4
10.4 10.7 16.2 13.8 13.6 13.9 14.6 10.9 9.7 8.6 8.2
25 16 10 6 8 11 17.5 22 25 28

-1.2 -0.3 -0.8 -0.5 0.0 +0.1 -0.6 -1.0 -1.1 -2.6 -3.8
6.1 5.2 5.7 5.4 4.9 4.8 5.5 5.9 6.0 7.5 8.7
30 13.5 12.5 9 6 11 12.5 18.5 25 30

-3.0 -2.7 -1.8 -0.5 0.0 -0.2 -2.1 -2.5 -3.5 -2.6 -3.4 -4.2
2.8 7.5 6.6 5.3 4.8 5.0 5.0 7.3 8.3 7.4 8.2 7.0
30 25 18 11 9 15.13 17 18 19 25 30

-3.5 -4.6 -2.2 +0.2 0.0 -0.3 -2.6 -4.3 -4.6 -7.9
6.6 9.7 23.4 2 5.1 5.4 -7.7 -2.5 9.7 12.1
Swale 50 14 10. 28 100

-2.8 -2.9 -2.1 -1.1 -0.3 0.0 -0.1 -1.5 -2.1 -2.9 -2.6 -2.5
8.3 2.1 3.8 8.6 5.8 5.5 5.6 9.0 7.6 8.1 8.1 9.0 2.6
30 23.5 22.5 18.6 11.5 10 11.5 16 15 18.5 24 30

4.1 1.6 -1.6 1.4 0.0 -0.6 -1.1 -2.1 -2.9
4.4 6.2 4.7 5.7 5.3 5.7 6.4 7.4 8.2
35 30 20 8 11 19 25 30

+3.9 +3.1 -0.3 -0.3 -0.7 0.0 -0.3 -0.9 +0.7 +0.7
2.0 2.8 4.2 4.2 4.6 3.9 4.2 4.8 3.2 3.2
30 25 22 14 13 11 12 14 30

+7.4 +6.1 +3.0 +1.0 -0.2 -0.4 0.0 0.0 -0.7 0.0 +2.7 +2.2 +1.4
5.2 2 9.6 16.6 13.8 13.0 12.6 12.6 13.3 12.6 10.9 10.5 11.5
trees 33 28 22 18 10.5 9 8 12 14.5 22 30

+4.2 +6.0 +2.0 +2.1 -0.6 -0.2 0.0 -0.3 -0.7 +2.2 +3.0 +3.5
0.5 4.1 5.9 6.6 5.3 2.7 2.7 3.0 3.4 5.5 4.7 4.2
trees 5 28 18 14 12 7 7 11 16 22 trees 30

+2.8 +3.3 +2.7 0.6 -0.2 0.0 -0.3 -1.0 +1.8 +2.4 +2.1
+4.0 1.0 2.0 5.3 4.9 4.7 5.0 5.7 2.9 2.3 2.6
33 28 22 12 8 0 5.5 10 14 19.5 25
T 7

+2.8 +1.0 +2.0 -1.1 -0.4 0.0 +0.4 -1.2 +0.7 +1.5 +0.1
+5.3 +5.0 0.0 3.1 2.4 3.0 2.4 3.2 6.3 6.5 4.9
33 26 17.5 18 8 5.5 10 13.5 19 25
T 7

127595

144		2.8	1243.2
+90			
+40		5.2	1240.8
145		8.9	1237.1
	3.44	1240.99	8.92
+45		3.6	1236.9
+55	Stone Box Good	1/2 span	1236.8 1232.0
+65		4.1	1236.4
146		4.1	1236.4
	12.36	1249.39	8.46
147		9.6	1239.8
B.N.R. 147-60		3.57	1245.82
+50		6.8	1242.6
148		4.8	1244.6
149		7.5	1241.9
150		9.4	1240.0
	6.24	1238.66	10.97
151		3.2	1235.5

+81	+73	+2.8	-1.1	0.0	0.0	-0.4	-1.2	+2.0	+1.9	+0.6
+5.3	+4.5	2.0	3.9	3.8	2.8	3.2	4.0	0.8	0.9	2.2
Tr. 33	25	18	12.5	7	0	5	9.5	14.5	19	25
+7.7	+7.2	+5.2	+1.6	-0.3	+0.1	0.0	-0.3	-1.0	+2.0	+3.2
+2.5	+2.0	2.0	3.0	5.5	5.1	5.2	5.5	6.2	3.2	2.0
Tr. 33	26.5	22	18.5	14	8	0	5	10	14	18.5
+1.4	-1.2	-1.2	-0.7	0.0	0.0	-0.3	-1.2	-1.8	-2.7	-4.7
Tr. 33	2.5	10.1	10.1	9.6	8.9	8.9	9.2	10.1	10.7	11.6
Tr. 33	22	14	12	8	0	5	9.5	16.8	19	25
-2.9	-2.8	-2.4	-0.7	0.0	0.0	-0.7	-3.9	-5.5		
Tr. 33	6.5	6.4	6.0	4.3	3.6	4.3	3.5	4.9		
Tr. 33	33	25	19	13	3.6	4.5	19	35		
-3.4	+1.4	+0.7	+0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Tr. 33	7.1	8.1	5.3	5.2	2.7	3.7	3.7	6.0	8.9	10.5
Tr. 33	34	16.6	15	7	7	7	7	10.5	11.2	5.0
-2.3	-1.5	+0.1	0.0	0.0	0.0	-0.7	-1.6	-2.6		
Tr. 33	6.4	5.6	4.0	4.1	4.1	4.8	5.7	6.7		
Tr. 33	30	18	11	8.5	10	12	25			
-1.7	-0.7	-0.4	-0.3	-0.2	0.0	-0.4	-1.1	-0.7	-0.7	+1.3
Tr. 33	5.8	4.8	4.5	4.8	4.3	4.1	4.5	5.2	4.8	4.8
Tr. 33	33	20	15	13.5	10	5	5.7	11	18	25
+5.4	+5.2	+4.0	-0.9	-0.4	0.0	-0.4	-0.9	+2.9	+3.4	+2.9
Tr. 33	4.2	4.4	5.0	16.5	10.0	9.6	10.0	10.5	6.7	6.2
Tr. 33	32	22	17	8	5	5	8.5	14	18.5	25
+6.5	+5.6	+4.3	-0.6	-0.1	0.0	-0.2	-0.8	+1.8	+2.2	+1.8
Tr. 33	4.3	1.2	2.5	7.4	6.9	6.8	7.0	7.6	5.0	4.6
Tr. 33	7.33	24	17	8	7	0	7	10	13	18.5
+3.4	+1.4	0.1	0.0	-0.1	-1.0	+0.2	0.0			
Tr. 33	4.7	3.4	4.9	4.8	4.9	5.8	4.6	4.8		
Tr. 33	31	15	11.5	6	12	18.5	25			
+3.5	+1.8	0.2	0.4	-0.9	0.1	0.0	-0.4	-0.9	-0.8	-1.1
Tr. 33	4.0	6.2	5.7	2.9	8.4	7.6	7.9	8.4	8.3	8.6
Tr. 33	31	19	14	13	7	7	7	11	19	25
+3.3	+1.9	-1.1	+0.3	0.0	-0.5	-1.1	-0.3	0.1	-0.4	
Tr. 33	6.1	7.5	10.5	9.4	9.9	10.5	9.7	9.5	9.8	
Tr. 33	33	19	14	6	7	11	13	3.0	2.5	
+3.2	+2.1	+1.1	+0.4	-0.5	-1.0	0.0	0.0	-0.1	-0.8	+2.4
Tr. 33	9.0	4.1	2.1	2.8	3.7	4.2	3.2	3.3	4.0	4.8
Tr. 33	38	22	19	16	14.5	12	9	6	9	13

1138.66

152		5.0	1233.7
+75		5.4	1233.3
+85	Stone Box Top Collapsing,	2 1/2' Span	1233.0 1229.9
153		5.5	1233.2
154		6.2	1232.5
155		4.2	1234.5
156		5.8	1232.9
157		11.2	1227.5
158	3.01	1229.75	11.92 1226.74
+36		4.7	1225.1
+46	Concrete Box Good Condition	25" Span	1225.1 1222.1
+56		4.9	1224.9
159		5.2	1224.6

+0.3	+0.2	+0.8	+0.7	-1.2	-1.3	+0.4	0.0	+0.3	-1.2	-1.1	0.1	+0.5	+0.5
4.7	5.2	5.8	5.7	6.2	6.3	5.4	5.0	5.3	6.2	6.1	5.1	4.5	4.5
33	27	28	16	14	12	9	12	5	9	13	14	20	25
-1.6	2.2	-1.5	-0.2	0.0	-0.1	-1.9	-2.6	-2.8	-2.8	-2.8	-2.8	-2.8	-2.8
3.0	2.0	6.9	5.6	5.4	5.5	2.3	8.0	8.2	8.2	8.2	8.2	8.2	8.2
33	21	15	12	12	9	9	14	22	25	25	25	25	25
-1.7	-2.2	-3.3	-1.7	+1.2	0.0	0.0	+0.3	-1.1	-1.3	-2.9	-3.6	+2.0	+2.0
7.4	7.9	9.0	6.9	4.5	5.7	5.7	5.4	4.6	7.0	8.6	9.3	9.7	9.7
60	32	15.0	15	15	4	4.0	4.0	25	50	25	50	50	50
-2.4	-2.0	-0.5	0.0	0.0	-0.1	-2.4	-2.5	-3.0	-2.5	-3.1	-3.1	-3.1	-3.1
2.9	8.1	6.0	5.5	5.5	5.6	7.9	8.0	8.5	8.0	8.6	8.6	8.6	8.6
33	19	12.5	6	6	5	8	11	12	14	25	30	30	30
+2.1	+1.1	-0.8	-1.0	-1.4	-1.4	-0.7	-0.1	0.0	-0.4	-1.1	-0.6	-0.3	-0.9
4.1	5.1	7.0	7.2	7.6	7.6	6.9	6.3	6.2	6.6	7.3	6.8	6.5	7.1
33	25	21	17	16	14	12	8	6	10	12	17	30	30
+3.0	+0.1	-0.5	+0.1	0.0	-0.3	-0.8	-0.3	-0.3	-0.2	-0.3	-0.2	-0.2	-0.2
1.2	4.1	4.7	4.3	4.2	4.5	5.0	4.8	4.5	4.4	4.5	4.4	4.4	4.4
33	15	14	9	9	10	13	17	25	30	30	30	30	30
+3.9	+3.1	-0.7	+0.2	0.0	+0.3	-0.7	+0.3	+0.3	+0.3	+0.5	+0.5	+0.5	+0.5
1.9	2.7	6.5	6.6	5.8	6.1	6.5	5.5	5.5	5.5	5.3	5.3	5.3	5.3
Tr	31	28	14	12	10	12.5	15	22	28	Tr	Tr	Tr	Tr
+5.5	+4.2	-0.4	0.0	0.0	-0.4	-1.2	+1.8	+2.1	+2.1	+2.1	+2.1	+2.1	+2.1
5.7	7.0	10.0	11.6	11.2	11.2	11.6	12.4	9.4	9.1	9.1	9.1	9.1	9.1
Tr	31	24	16	11.6	9	13	18	26	Tr	Tr	Tr	Tr	Tr
+0.3	+0.6	-0.6	-1.0	0.0	0.0	-0.7	+1.5	+1.0	+2.7	+2.7	+2.7	+2.7	+2.7
4.5	5.4	5.4	5.8	4.8	4.8	5.0	6.3	5.8	7.5	7.5	7.5	7.5	7.5
Tr	31	23	14	13	8	2	10	14	16	28	Tr	Tr	Tr
+0.3	-1.6	-1.6	-2.0	-0.2	0.0	0.0	-2.8	-2.2	-3.9	-3.9	-3.9	-3.9	-3.9
5.0	6.3	6.3	6.7	4.9	4.7	4.7	7.5	6.9	8.6	8.6	8.6	8.6	8.6
Tr	30	21	18	16	8	11	18	19	28	Tr	Tr	Tr	Tr
-1.3	-2.1	-2.8	-1.7	+0.8	0.0	0.0	+0.2	+0.7	+1.8	+3.1	+5.8	+8.0	+8.0
Valley	6.0	6.8	25-6A	29	4.7	4.7	4.5	4.0	6.5	28	10.3	12.7	12.7
No Ditch	50	17	9.2	7.5	11	12.6	11	12.6	28	7.5	ditch	ditch	ditch
+0.1	-1.1	1.7	-2.0	-0.3	0.0	0.0	-2.9	-3.5	-3.5	-3.5	-3.5	-3.5	-3.5
4.8	6.0	6.6	6.9	5.2	4.9	4.9	7.8	8.4	8.4	8.4	8.4	8.4	8.4
Tr	30	21	19	14	7	11	20	27	Tr	Tr	Tr	Tr	Tr
+3.7	+3.0	-1.5	-0.2	0.0	-0.2	-0.5	+1.6	+1.8	+3.5	+3.5	+3.5	+3.5	+3.5
4.5	2.2	6.7	6.7	5.4	5.2	5.4	5.7	6.8	7.0	8.7	8.7	8.7	8.7
Tr	29	22	14	8	4	5	10	14	18	29	Tr	Tr	Tr

1229.75

159+75 5.4 1224.3

160 6.1 1223.7

768 6.5 1223.3

+78 Stone Box, 2 1/2' E Span. 1223.4
Poor Condition, Sides & Top pushing in 1218.9

+88 6.3 1223.5

161 6.1 1223.7

12.35 1237.41 4.69 1225.06

162 12.0 1225.4

163 4.3 1233.1

6.82 1241.99 2.24 1235.17

+65 5.3 1236.7

164 6.6 1235.4

B.M. Left 164+25 1.32 1240.67

(1240.64)

+7.4	+6.6	-1.0	-0.1	0.0	+0.4	-0.1	-1.4	-0.9	-1.1
+2.0	+1.2	6.4	5.5	5.4	5.0	5.5	6.8	6.3	6.5
Tr. 28.5	19	7.5	3		6	11	17	18	28.70

+7.6	+7.1	-0.9	-1.2	-0.2	0.0	+0.4	-0.3	-1.2	-1.5	-1.1	-1.0	-2.0
+1.5	+1.0	2.0	2.3	6.3	6.1	5.7	6.4	7.3	7.6	7.2	7.1	8.1
Tr. 29	21	8	6	3		6	12	15	18	20	24	25.70

-1.5	-3.0	-2.0	-0.1	0.0	+0.2	-2.7	4.2	
8.0	7.5	8.5	6.6	6.5	6.7	9.2	10.7	
1 st Tree	27.5	16	11	5		13.5	19	30

+3.2	+2.15	+1.1	-0.1	0.0	+0.1	+0.8	-1.9	+4.1	-5.1	-7.4
9.6	10.7	9.5	6.5	6.4	6.3	5.8	8.3	11.1	11.5	13.8
27	30	7			13	15.1		30	8.5	

+3.1	+2.1	+1.9	-0.1	0.0	-0.2	-1.4	-2.5	-2.4	
7.4	8.9	8.7	8.2	6.4	6.3	6.5	7.7	8.8	8.7
27	24	16	13	6		14	16	20	27.7

+2.7	+2.3	+1.9	+1.7	0.0	0.0	+0.1	-1.4	+1.8	+1.7
9.0	8.4	8.0	7.9	6.1	6.1	6.2	7.2	8.0	8.8
27	24	16	13	6		14	16	20	27

+0.9	+1.3	+1.7	+1.5	+0.4	0.0	-0.5	-0.2	0.0	0.0	-0.2	-0.2	+4.5	+5.2
11.1	10.7	10.5	11.6	12.0	12.5	12.2		12.0	12.0	12.2	12.2	7.5	6.8
27	24	22	20	15	12.5	16	5		9	12	18	27	31

+2.8	+3.1	+1.6	+0.1	0.0	+0.3	-0.2	+3.3	+3.7	+4.0
4.5	4.2	2.7	6.4	4.3	4.0	4.5	4.0	0.6	0.3
Tr. 26.5	21	12	9		11	15	19	2.5	30

+3.6	+3.3	+2.5	+0.3	0.0	-0.1	+2.0	+2.1	+2.0
1.7	2.0	2.8	5.0	3.3	5.4	3.3	3.2	3.3
26	18	11.5	7		16	23	27	30

+3.8	+3.6	+1.7	+0.7	+0.2	0.0	+0.1	+0.1	+1.9
2.8	3.0	4.9	5.9	6.4	6.6	6.5	6.7	7.7
30	19	10	6	4.5		12	15	30

~~Tr. B~~

0.38 1241.72 1240.4

164 170 11.7 1229.3

165 13.1 1227.9

0.30 1228.90 1242 1228.60

166 4.1 1224.8

167 7.5 1221.4

168 10.3 1218.6

2.84 1220.65 11.11 1217.79

169 6.6 1214.1

170 7.2 1213.5

2 1/2' x 3' Stone Box, Foot 15" Wide at W. End
+06.5 Walls Slanted Together in Center. 1218.8
1208.8

+15 6.8 1213.7

171 6.0 1214.7

10.13 1229.98 0.80 1219.85

172 11.4 1218.6

+50 7.3 1222.7

7.75 $\frac{1}{2}$ Cross Roads 5.4 1224.6

Nov. 2, 1923, Marks
Fair, Cool. Thompson } Day
Grady. }
Exp. Marks. 31
Dinners, 1.50
Auto 22/10ml, 2.70

BM L. 164 + 2.7
+3.7 +2.7 +2.1 +0.6 +0.2 -0.3 0.0 0.0 0.3 +1.4 +3.6
8.0 7.0 7.0 11.1 11.5 11.5 11.7 11.7 12.0 10.3 8.1
14.12 9.65 4.5 4
+3.2 +2.4 0.0 -0.6 0.0 +0.2 -0.5 +0.1 +0.9 +1.6
9.9 10.7 13.1 13.7 13.1 12.9 13.6 13.0 12.2 11.5
Tr. 2 2 12 7 4 15 19 19.5 25 30
+0.6 +0.1 +0.4 0.9 +0.2 0.0 +0.3 -0.1 -1.0 0.4 -0.8 -0.8
3.5 4.0 4.5 5.0 3.9 4.1 3.8 4.2 5.1 4.5 4.9 4.9
Tr. 23 18.5 6 5 2 13 18 21 22 25 30
+3.0 +2.0 +1.5 +0.8 +0.1 -0.6 0.0 0.0 +0.2 +0.4 +0.5 +0.6 +0.5
4.5 4.5 5.0 6.7 7.4 6.1 7.5 7.5 7.3 7.9 7.0 6.9 7.0
20 18.5 10 7 5. 4 2 13 19 22 25 30
Tr. 2
+5.0 +4.3 -0.8 -1.5 -0.2 0.0 +0.8 -0.9 -1.5 +2.1 +3.1
3.3 6.0 11.1 11.8 10.5 10.3 11.1 11.2 11.8 8.2 9.2
Tr. 20 14 6 4 2 9 16 17 22 30
+3.7 +2.8 -0.4 0.0 +0.1 +0.1 -0.4 0.0 +1.4 +1.6
2.9 3.8 7.0 6.6 6.5 6.5 7.0 6.6 5.2 5.0
8.2 20 5 9 7 16 19 20 25 30
-2.2 -1.7 3.0 2.5 0.2 0.0 0.0 -1.2 2.2 2.2 -2.9
1.4 8.9 10.2 9.7 7.4 7.2 7.2 8.4 10.4 9.4 10.1
21 11 9 5 3 16 20 24 27 31
-1.7 +1.3 +8 -2.1 +0.2 0.0 -0.2 -1.5 5.2 -5.4 7.3
8.6 11.2 11.7 9.0 6.7 9.9 7.1 7.4 12.1 12.3 14.2
10.0 20 51 116 35 100
-2.2 -1.7 +1.4 3.2 2.0 -0.2 0.0 +0.3 -0.1 -1.6 -3.5 2.4 -3.2
9.0 8.5 8.2 16.0 3.8 7.0 6.8 6.5 6.7 8.4 10.3 9.2 10.0
30 21 14 12 10 2 9 17 20 25 30 32
+4.0 +3.8 +3.2 0.4 0.6 0.1 0.0 +0.1 0.4 -0.9 +0.6 +1.4 +2.0
3.0 3.2 2.8 6.2 6.6 6.1 6.0 5.9 6.5 6.9 5.4 4.6 4.0
30 22 20 13 7 5 7 16 18.5 22 25 33 Fence
+6.2 +6.6 +6.4 -0.4 +0.0 -0.4 0.0 -0.1 -0.3 -0.8 +1.4 +1.7 +5.0
4.5 4.9 5.0 11.8 12.4 11.8 11.4 11.5 11.7 12.2 7.0 6.7 6.4
30 24 19 8 6 5 7 15 16 25 30 34 Fence
+6.0 +5.5 +0.9 0.0 +0.9 +1.5 +1.8
1.3 1.8 6.4 7.3 7.6 8.2 5.8 5.5
30 21 9 13 19 26 39
+10.2 +7.2 +5.4 +2.7 0.0 -0.7 -0.4 -0.3 +0.4 +0.6 -0.9
+4.8 +1.8 0.0 3.7 5.4 6.1 5.9 5.7 5.0 4.8 6.3
150 100 50 19 5.4 72 32 50 100 100 200

1229.92

173 4.1 1225.9

174 1.9 1228.1

B.M. F. 173705 322 1226.76

175 4.7 1225.3

+75 2.95 1227.55 5.43 1224.55

176 3.7 1223.8

+50 5.8 1221.7

177 9.9 1217.6

+15 11.8 1215.7
+50 13.0 1214.5

185 1217.25 1210 1215.40

178 4.3 1213.0

+57.5

+64 stone Boy V. End 18" 1212.1
+67.5 Fall E. End 30" 1207.3

+77.5 5.4 1211.9

445 1212.80

179 5.3 1212.0

180 2.6 1214.7

11.79 1228.30 0.74 1216.51

+5.1 +4.6 0.0 0.0 -0.7 -0.3
+1.0 +0.5 4.13 4.1 4.8 4.4
30 21 16 12 0 30 35 tree line

+3.1 2.9 2.3 1.2 0.3 0.0 -0.4 -1.3 -1.1 -1.5
+1.2 +1.0 +0.4 3.1 2.2 1.9 2.3 3.2 3.0 3.4
30 21 17 10.5 7 8 18 25 32 7

+4.7 +4.0 +3.1 0.7 0.3 0.0 +0.1 0.5 0.0 0.2 0.5
0.0 0.7 1.6 5.4 5.0 4.7 4.6 5.2 4.7 4.9 5.2
30 21 17.5 10 7 8 18 19 23 30

+1.3 +1.3 +0.6 1.4 0.3 0.0 0.1 1.0 0.1 0.9 1.0
R.4 2.4 3.1 5.1 4.0 3.7 3.8 4.7 3.8 3.8 4.7
30 21 13.5 10 6.5 7 16 17 25 29

+7.4 7.4 +0.3 0.7 0.1 0.0 0.0 0.5 +5.4 +5.9
2.5 2.5 3.6 10.6 10.0 7.9 9.9 14.4 10.5 8.0
30 22 14 8 5 13 15 25 31

-0.5 -1.2 0.9 -1.2 0.6 0.0 +0.2 -0.3 0.7 2.6 3.4
3.2 5.5 5.2 5.5 4.9 4.3 4.1 5.1 5.0 6.9 7.7
30 24 11 7 6 6 14 18 25 29

Same as +77.5

-1.9 -4.8 -1.8 0.8 -0.1 0.0 +0.2 +0.6 -2.0 -4.8 -5.9 -6.3
7.1 4.0 2.0 9.2 5.3 5.2 5.0 4.6 7.2 10.0 11.1 11.5
Swale 50 8.2 6 12.5 14.5 27 73

-2.7 -1.6 -1.0 -0.4 0.0 0.0 -0.9 -2.3
8.1 7.0 6.4 5.8 5.7 5.4 6.3 7.7
30 26 21 8 6 15 16 30

N.W. cor. W. H. W.

-1.4 1.1 -0.4 0.6 0.0 -0.2 0.8 0.5 1.2 0.7
6.7 6.4 5.7 5.9 5.3 5.5 6.1 5.8 6.5 6.0
30 23 19 8 7 12 16 17 25 30

+0.8 +0.5 +0.8 -0.1 -0.3 0.0 +0.1 -0.2 -1.0 -0.6 -0.2 -1.9 +3.0
1.8 1.8 1.8 1.7 3.4 2.6 2.5 2.8 3.6 3.2 2.8 0.7 +0.7
30 22 14.5 10.5 7 6 11 14 16 18 22 28

1228.30

181			6.6	1221.7
+60	6.95	1234.35	0.70	1227.40
+80			6.9	1227.4
			5.3	1229.0
182			5.1	1229.2
183			10.6	1223.7
	1.36	1223.23	12.48	1221.87
184			4.2	1219.0
185			6.3	1216.9
+33				
+43	Stone Box	W. End, 2 1/4' span		1217.1
	Fair	E. " 3 1/2' "		1212.8
+53			6.1	1217.1
186			5.9	1217.3
	8.87	1230.50	1.60	1221.63
187			8.6	1221.9
+40			5.8	1224.7

	+A.2	+3.7	-0.6	0.0	0.0	-0.6	+3.6	+4.3						
	2.4	2.9	2.2	6.6	6.6	7.2	3.0	2.3						
Tr.	19.5	15	8		6	14	22	26	Tr.					
	+A.4	+3.9	+0.8	-0.6	0.0	+0.1	+0.4	+3.1	+3.5					
	2.5	3.0	6.1	7.5	6.9	6.8	7.3	3.8	3.4					
Tr.	39	14	11	7	11	15	19.5	26	Tr.					
	+2.9	+2.2	-0.4	0.0	0.0	-0.6	+3.5	+3.7						
	2.4	3.1	3.7	5.3	5.3	5.9	4.8	1.6						
Tr.	30.5	17	7		6	15	23	26	Tr.					
	+2.0	+0.0	+0.0	-0.4	0.8	+0.3	+2.1	+3.0						
	3.0	5.0	5.0	5.1	5.8	4.7	3.9	2.0						
Tr.	31	11	9	16	18.5	22	28	Tr.						
	+2.7	+2.6	-1.0	-0.5	0.0	0.0	-1.0	+0.1	+1.1	+4.3				
	7.9	8.0	11.6	11.1	10.6	10.6	16.0	11.6	10.5	6.5	6.3			
Tr.	25.5	17	10	7		10	14	15.5	17	23	27	Tr.		
	+2.1	+2.5	+0.3	+0.0	-0.4	0.0	+0.1	-0.1	-0.7	+0.1	+0.4	+1.8	+2.2	
	1.1	0.7	3.9	5.2	5.2	4.6	7.2	4.1	4.3	4.9	4.1	5.8	2.4	2.0
Tr.	27	20	15	9	6	5.5	8	12	14	17	23	25	31	Tr.
	-0.9	-1.1	-0.4	-0.6	0.0	+0.3	-0.1	-0.7	-0.7	-1.9	-2.4			
	7.2	7.4	6.7	6.9	6.3	6.0	3.0	7.0	7.8	8.2	8.7			
	30	18	9	8		8	16	17	20	27	30			
	Same as +53													
	-2.4	-2.9	-1.4	-2.2	+0.5	-0.1	0.0							
	8.5	9.0	10.5	8.3	5.6	6.2	6.1							
	50	25		9.6	8									
	-2.4	-1.5	-3.0	-0.2	0.0	0.2	-2.6	-2.0	-2.8	-3.0				
	8.5	7.6	9.1	6.3	6.1	6.3	8.7	8.1	8.9	9.1				
	38	24	15	13	7	14	20	23	28	30				
	-1.4	-0.3	-0.7	0.0	0.0	-0.6	-0.3	-1.7	-1.4					
	7.3	6.2	6.6	5.9	5.9	6.5	6.2	7.6	7.3					
	30	11	9		9	14	18	25	30					
	+5.1	+4.2	0.0	-0.3	-1.3	-0.1	0.0	+0.4	-0.3	+2.3	+1.2	+7.5		
	3.5	4.5	8.6	8.9	9.4	9.9	8.7	8.6	8.2	6.9	6.3	3.4	1.1	
	30	24	18	12	11.5	9	8	12	12	20	26	33		
	+3.3	+2.8	-1.0	+0.2	-1.7	-0.4	0.0	+0.2	-0.5	-0.2	+1.6	+2.7	+4.2	
	2.5	3.0	6.8	5.6	8.5	6.2	5.8	6.6	6.4	6.0	4.2	3.1	1.6	
	30	24	19	17	15	14	12	14	16	18.5	25	30		

12 30 50

		2.42	1228.08	(1228.10)
188		4.0	1226.5	
189		3.8	1226.7	
190	8.52 1236.87	2.15	1228.35	
		8.7	1228.2	
191		7.6	1229.3	
	+45	7.6	1229.3	
192		7.7	1229.2	
193		6.8	1230.1	
194		4.5	1232.4	
	+25	4.2	1232.7	
195		9.3	1227.6	
	0.74 1225.14	12.47	1224.40	
196		4.7	1220.4	
197		9.2	1215.9	
	4.00 1219.10	10.38	1214.76	

B. M. R. 187780

-0.5	-0.5	1.3	-0.5	0.0	-0.2	-1.1	-0.4
4.5	4.5	5.3	4.5	4.0	4.2	5.1	4.4
30	16.5	70	6	8	16	30	
+1.7	+1.0	-0.2	-0.5	-1.0	0.0	-0.1	-1.7
2.1	3.8	4.0	4.3	4.8	3.8	3.9	5.0
30	23	19	70	9	8	17	18.21
+3.1	+1.8	-0.3	-0.8	-1.3	-0.5	0.0	+0.3
5.6	6.9	9.0	9.5	10.0	9.2	8.7	8.4
30	18	15	4	10	8	6	12
+2.3	+0.2	-1.2	-0.5	0.0	+0.1	-0.6	-1.0
5.3	7.4	8.8	8.1	7.6	7.5	8.2	8.6
30	18	12	9	6	13	16	22
+2.9	+1.1	-0.1	-0.3	-1.0	0.0	-0.2	-0.9
4.7	6.5	7.7	7.9	8.6	7.6	7.8	8.5
30	18	16	13	4	11	17	18
+3.1	+2.3	-0.6	-0.3	0.0	-0.1	-0.8	-0.1
4.6	5.4	8.3	8.0	7.7	7.8	8.5	7.8
30	23	11	9	9	16	18	30
+1.4	-0.3	-0.9	0.0	+0.1	-0.7	+0.3	
5.7	7.1	7.7	6.8	6.7	6.5	6.5	
30	17	11	6	16	30		
+2.6	+2.6	+0.3	-0.1	-0.8	0.0	-0.1	-0.5
1.4	1.4	2.2	4.6	5.3	4.5	4.6	5.0
30	22	16	12	11	4	16	22
+3.4	+3.0	+0.2	-0.1	-1.0	-0.3	0.0	-0.3
0.8	1.3	4.0	4.5	5.2	4.5	4.2	4.5
30	21	13	12	11	8	13	16
+3.8	+3.5	+0.4	-0.5	-0.1	0.0	-0.3	+1.0
5.5	5.8	8.9	9.8	9.4	9.3	9.6	8.3
Tr 24.5	21	11	10	7	15	16	23
+4.1	+4.3	-0.8	-0.1	0.0	+0.1	-0.3	-0.8
30	30	14	5.5	4.8	4.7	4.6	5.0
	25	20	10	6	5	13	15
+1.4	+1.9	-0.6	+0.1	-0.3	0.0	+0.1	-0.4
2.8	3.5	2.5	7.1	7.5	7.2	7.1	7.6
30	23	12	8	7	4	12	14

N.F. CT. B-H.K. 1897+80

1226.36

205 7.6 1218.8

206 6.9 1219.5

11.81 1231.09 7.08 1219.58

5744C Box SPRN, E. End 2.5" 1219.5
+0.5.5 Fair, 2 Lebs Broken W. 2.5" 1215.7

+15

207 11.9 1219.2

208 9.1 1222.0

209 6.1 1225.0

210 3.8 1227.3

+75 1.6 1229.5

211 1.7 1229.4

212 2.8 1228.3

9.02 1235.25 2.86 1228.28

213 7.7 1227.8

213+0.76 1/2" Sec. C.1. 7.3 1227.9
9.7 1225.5

213-15

+1.6 +1.1 +1.3 -0.4 0.9 -0.2 0.0 +0.3 -0.2 -0.9 0.5 -0.5 +0.2
6.5 6.5 6.3 8.0 8.5 7.8 7.6 7.3 7.8 8.5 8.1 8.1 8.4
30 22 17 46 6.5 2.5 9 17 19 30.5 25 30

+2.1 -2.1 -2.2 3.0 -2.5 -0.2 0.0 -0.4 3.0 -2.2 -2.4
9.0 9.0 9.1 8.9 7.4 7.1 6.9 7.3 9.9 9.1 9.2
30 23 13 11 5 1 15.5 22 25 30

-2.5 +3.8 +4.2 0.3 0.0 -0.3 -1.3 3.8 3.9
14.1 15.4 12.8 11.9 11.6 11.9 12.0 15.4 15.5
25 33 17.3 50

Same as 206+0.0

+1.0 +1.0 +0.5 -0.1 -0.0 0.0 +0.4 -0.1 +1.3 1.0 0.2
10.9 10.9 10.4 12.0 12.5 11.9 11.5 12.0 13.2 12.1 12.1
30 20.5 14 13 7 8 18.5 19.5 30.5 30

+2.1 +1.1 +3.6 +2.4 +0.5 -0.3 0.0 0.0 -0.6 +0.4 +1.8 +1.6
5.9 5.0 5.5 6.7 8.6 9.4 7.1 7.1 7.7 8.7 7.3 7.5
30 25 17 11 8 9 17 22 23 31

+1.5 +1.2 0.0 -0.2 -0.9 0.3 0.0 0.0 -0.2 -0.6 +1.0 +1.1
6.9 6.1 6.3 7.0 6.4 6.1 6.1 6.3 6.7 5.1 5.0
30 13.5 7 8 6.5 4 7 16 17 25 32

+2.0 +1.7 +0.3 -0.7 -0.1 0.0 0.0 +0.1 -0.5 0.0
7.9 7.2 7.5 4.5 3.9 3.8 3.7 4.5 3.8
30 16 9 7 4 17 31

+3.6 +2.3 -0.8 -0.9 -1.4 -0.5 0.0 0.0 -0.5 -1.2 -0.7 -1.3
7.5 7.5 7.4 2.5 3.0 2.1 1.6 1.6 2.1 2.8 2.3 2.9
30 30 15 10 8 5 5 16 18 20 31

+1.7 +1.6 +1.5 -0.5 +1.3 -0.3 0.0 +0.1 -0.5 -1.0 0.5 -0.3 -0.6
0.1 0.2 2.9 3.0 2.0 1.7 1.6 2.2 2.7 2.2 2.0 2.3
30 2 18 13 11 10 6 6 15 18.5 18 29 31

+1.7 +1.5 -0.7 -1.2 -0.5 0.0 -0.6 -1.2 -0.8 -0.3 -0.4
1.1 1.3 3.5 4.0 3.3 2.8 2.4 4.0 3.6 3.1 3.2
30 19 2 9 8 16 16 19 25 30

-0.2 -0.2 -1.0 -2.0 -1.0 0.0 0.0 -0.1 -1.8 -2.0 -1.2 -2.1 2.5
7.0 7.6 8.4 9.7 8.6 7.4 7.7 7.5 7.2 7.4 5.6 7.5 8.9
30 23 15 15 14 8 11 16 18 20 25 30

-0.3 -0.7 2.1 0.0 0.0 -0.3 2.7 3.1 2.7
7.5 8.0 7.7 7.8 7.3 7.6 10.0 10.4 12.0
50 25 5.1 8.3 11.7 25 50

Same as 213+0.0

123525

214 6.9 1228.3

215 4.7 1230.6

+60 3.8 1231.4

216 B.M. 3.7 1231.5

L. 216+ 1.07 1236.00 0.32 1239.93 (1234.7)

217 7.0 1229.0

+60 7.2 1228.8

+70 34" Concrete Box 7.3 1228.7
Good Condition 11.1 1224.9

+80 7.2 1228.8

218 7.3 1228.7

219 6.5 1229.5

220 4.0 1232.0

221 2.7 1233.3

+60 1.8 1234.2

+2.3 +2.3 +2.0 -0.1 -0.4 -1.0 -0.5 0.0 +0.1 -0.4 -0.9 -0.3 +0.2 +0.5

4.6	4.6	4.9	7.0	7.3	7.9	7.4	6.9	6.8	7.3	7.8	7.2	6.7	6.4
30	25	24	14	11	10	8	5	13	15	16	19	30	

+0.6 +0.1 -0.7 -0.2 -0.0 -0.3 -0.8 -0.3 -0.3

4.1	4.6	5.4	6.9	4.7	5.0	5.5	5.0	5.0					
30	13	12	10	13	14	15	30						

0.0 -0.2 -0.6 0.0 -0.3 -0.9 -0.4 +0.3 -0.6

3.8	4.0	4.4	5.8	4.1	4.7	4.2	3.5	4.4					
30	14	11.5		12	13	14	23	30					

+2.7 +2.2 +1.4 -0.1 0.0 -0.2 -0.5 +0.5 +1.5 +1.7

10	15	2.3	3.8	2.7	3.9	4.2	3.2	2.2	2.0				
30	21.5	15	11.5	12	12.5	16	25	30	30	Boon			

+3.0 +2.5 -0.2 -0.6 0.0 0.0 -0.4 -0.5 -0.4 -1.4

4.0	4.5	3.2	7.6	7.0	9.0	7.4	7.8	8.4					
30	25	19	14.5	11	12	13	14	30					

Sum 2.3 + 80

-2.9 -3.9 -1.65 +0.2 0.0 -0.15 -2.07 -3.7 -3.7 -4.6

12.2	11.2	8.95	7.0	7.3	7.5	9.37	4.0	11.0	1.9
25		14.9				11.7		2.5	50

-2.0 -1.2 -0.2 0.0 -0.2 -1.7 -2.2 -2.3 -2.3

9.2	8.4	7.4	7.2	7.4	8.9	9.4	9.5	9.5					
30	12	9		11.5	15.5	17.2	28	30					

-0.7 -0.7 -1.1 -0.5 +1.1 -0.4 0.0 -0.7 -1.3 -0.7 -1.3 -1.8

8.0	8.4	7.8	8.4	7.7	8.3	8.0	8.0	8.0	8.6	9.1			
30	25	22	11.5	9	12	13	14	19	30				

+1.6 +0.7 -0.2 -0.8 -0.4 0.0 -0.2 -0.6 0.0 +0.7 +0.9

4.9	5.8	6.7	7.3	6.9	6.5	6.7	7.1	6.5	5.8	5.6			
30-26	19	14	11	10		10	12	13	18	30			

+1.6 +0.8 -0.4 -1.0 -0.4 0.0 -0.5 -0.8 -0.5 -0.1 -0.4

1.4	3.2	4.4	5.2	4.4	4.0	4.5	4.8	4.5	4.1	4.4			
30	17	15	13	12.5	11	10	11.5	12	14	30			

+1.6 +0.4 -0.5 -0.1 0.0 -0.1 +0.5 +1.1

1.1	2.3	3.2	2.8	2.7	3.8	2.2	1.6						
30	14	13	12		12	13	50						

+1.8 -0.1 -0.4 0.0 -0.5 +0.1 +0.8 +1.2

0.0	1.9	2.2	1.8	2.5	1.7	1.0	0.6						
30	17	13		12.5	14	18	30						

1236.00

2 2 2 2.5 1233.5

2 2 3 3.3 1232.7

3.89 1236.93 2.96 1233.04
+13 E Cross Roads 4.5 1232.4

2 1 4 6.7 1230.2

B.M. L. 2 2 4 4 3.95 1234.56 6.32 1230.61 (1230.59)

2 1 5 5.8 1228.8

+27 18" x 12" Plank Culvert, Unservicable 1229.7 1226.2

+50 6.0 1228.6

2 2 6 5.5 1229.1

2 2 7 8.5 1226.1

2 2 8 9.7 1224.9

+30 9.5 1225.1

+40 stone Box E. End 2'8" Wide 1225.1
Good W. End 2'8" 1221.6

9.5 1225.1

+50 1225.1

+1.0 +0.9 +0.1 -0.6 -0.2 0.0 -0.7 0.0 +0.7 +1.4
1.5 1.6 2.4 3.1 2.7 1.5 3.2 2.5 7.8 1.1
30 18 14 13 12 11 12 15 30

+0.8 -0.2 +1.2 +0.3 0.0 -0.4 -0.1 -0.1
2.5 3.5 1.1 3.0 3.3 3.7 3.1 3.4
30 22 17 13 15 25 30

+6.0 +2.5 0.0 0.0 +1.1 +3.9 +1.9
1.5 2.0 4.5 4.5 3.4 0.8 2.6
30 100 25 100 200 320

+2.9 +2.2 0.0 -0.8 -0.2 0.0 -0.5 -1.7 -1.1 +1.2 +1.7 +2.5
3.8 4.5 6.7 7.5 6.9 6.7 7.2 8.4 7.8 5.5 5.0 4.2
30 26 22 15 13 10 12 15 17 30 30

0.0 +0.2 -1.2 0.0 0.0 -0.2 -0.8 -0.2 -1.1
5.8 5.6 7.5 5.8 5.8 6.0 8.6 8.0 6.9
30 18 12 12 9 13 14 30

-1.0 -2.3 0.0 0.0 +0.1 -2.7 -3.3 -3.7
6.7 8.2 5.9 5.9 5.8 8.6 9.2 9.6
30 4 11 7 10 30 50

+3.0 +2.4 -0.2 0.0 -0.4 -2.0
3.0 3.6 5.2 6.0 6.4 8.0
30 26 18 14 30

+3.8 +3.1 0.0 -0.5 -0.2 0.0 +0.2 -0.5
1.7 2.4 5.5 6.0 5.7 5.5 5.3 6.0
30 25 12 17 27 30

+3.4 +0.3 -0.3 +0.2 0.0 -0.4 +0.5 -0.1
5.1 8.2 8.8 8.3 8.5 8.9 8.0 5.6
30 16 13 13 13 22 28

+1.7 -1.2 -1.1 -0.3 0.0 0.0 -0.8 -0.4 -1.8 -2.4
8.0 10.8 10.8 10.0 9.7 9.7 10.5 10.1 11.5 12.1
30 22 17 12 9.5 11 12 20 25-30

Same as +50

-1.3 -3.6 -1.6 +0.9 0.0 0.0 +0.1 +0.8 -1.7 -3.5 -AA -AA
11.3 13.1 11.1 8.6 9.5 9.5 9.4 8.7 11.2 13.0 13.9 13.9
30 20 12 11.5 7.8 21 30

-1.7 -2.0 -2.8 -2.0 -1.8 0.1 0.0 0.0 -2.0 -2.3 -2.5
11.2 11.5 13.3 14.3 11.3 9.6 9.5 9.5 11.5 11.8 12.0
30 19 18 16 14 11 7 12 22 30

1234.56

229 9.4 1225.2

230 7.7 1226.9

231 4.71 1235.76 3.51 1231.05
5.1 1230.7

232 3.5 1232.3

233 9.0 1231.8

234 5.1 1230.7
5.51 1230.25

11.91 1242.16 1230.25

234+90 12" c.l. culvert 11.1 1231.1

234+80 230 11.0 1231.2

236 9.4 1232.8

237 6.2 1236.0

+60 2.5 1239.7

238 3.6 1238.6

-0.3 -0.5 -0.9 -0.4 0.0 -0.5 -0.8 -0.6

9.7 9.9 10.3 9.8 9.4 9.9 10.2 10.0

30 17 15 14 12 25 30

+3.9 +2.5 -0.5 0.0 -0.5 +0.2 -0.1 -0.3

3.8 5.2 8.2 7.7 8.2 7.5 2.8 3.8

30 22 16 13 13 23 25 30

+4.1 +3.3 -0.6 -0.1 0.0 -0.5 -0.5 +0.4 +0.4 +0.1

1.0 1.8 5.7 5.2 5.1 5.6 5.0 4.7 4.7 5.0

30 22 16 13 11 14 16 23 30

+1.7 +0.8 -0.9 -0.3 +0.1 0.0 -0.5 -1.2 -1.1 -1.6 -2.3

1.8 2.7 4.4 3.8 2.4 3.5 4.0 4.7 4.6 5.1 5.8

31 31 16 12 7 9 12 13 23 30

+2.8 +2.1 +0.1 -0.4 -0.9 -0.4 +0.1 0.0 -0.3 -1.1 -0.6 -0.4 -0.4 -1.3

1.2 1.9 3.9 4.4 3.9 4.4 3.9 4.0 4.3 5.1 4.6 4.4 4.4 3.3

28 24 19 16 15 13 6 10 11 12 17 20 30

+1.0 -0.1 -0.3 -0.7 -0.5 +0.1 0.0 -0.2 -0.9 -0.6 -1.6

4.1 5.2 5.4 5.8 5.6 5.0 5.1 5.3 5.0 5.7 6.7

30 23 17 16 14 5 10 12 13 30

W. End. C.l. Pipe Culvert, 234+90

Dec. 3, 1923 Marks

Fall Gray
Thomson

-1.4 -2.0 -0.6 -0.3 0.0 -0.3 -1.5 -2.7 -2.2 +1

11.5 13.1 11.9 14 11.1 11.4 12.6 13.8 13.3 15.2

100 7 7 9.1 2.0 2.5 100

Ground

-0.3 -1.5 -0.3 0.0 -0.2 -1.3 -1.8

11.3 11.5 11.3 11.0 11.2 12.3 12.8 11.3

30-25 19-16 12 7 12 25-30

+2.4 +1.0 -0.6 -0.1 0.0 -0.1 -0.6 -0.3 -0.2 +1.6 +1.9

9.0 8.5 10.0 9.5 9.4 9.5 10.0 9.7 9.6 7.8 7.5

28 18 15 13 0 11 12 13 15 22 25-30

+2.3 +2.9 -0.1 0.0 +0.2 +3.0 +3.2

3.9 3.3 6.3 6.2 6.0 3.2 3.0

30 21 15 11 19 30

+1.3 +0.7 +0.2 -0.3 0.0 +0.4 +1.3 +1.5 +1.7

1.2 1.8 2.3 2.8 2.5 2.1 1.2 1.0 0.8

30 19 15 14 0 11 18 25 27.5

+2.0 +1.3 +0.3 -0.4 +0.1 0.0 -0.4 -0.7 +1.3 +1.0

1.6 2.3 3.3 4.0 3.5 3.6 4.0 4.3 2.6

30 24 15 14 9 4 4 17 25-30

1242.16

3.48 1238.68 (1238.62)

5.91 1244.53

1238.62

239

6.1 1238.4

+25 4" Tife

6.2 1238.3
7.6 1236.9

240

5.8 1238.7

+50

5.2 1239.3

+85

3.9 1240.6

241

4.5 1240.0

242

6.9 1237.6

243

9.8 1234.7

4.05 1236.62

11.96 1232.57

244

5.0 1231.6

243+50

3.9 1232.7

243+25

4.4 1232.2

244+31.5 Stone Box

5 pan E Eng 2.7 1231.2
W. Eng 2.2 1227.1

W. Half, Poor Condition

B.M.E / m. L. 238 + 75

$$\begin{array}{r}
-0.4 \quad -0.8 \quad -1.0 \quad -0.4 \quad 0.0 \quad -0.5 \quad -1.4 \quad -1.0 \quad -1.4 \quad -1.8 \\
6.5 \quad 6.9 \quad 7.1 \quad 6.5 \quad 6.1 \quad 6.6 \quad 7.3 \quad 7.1 \quad 7.5 \quad 7.9 \\
30 \quad 75 \quad 12 \quad 11 \quad \quad \quad 8 \quad 11 \quad 12 \quad 25 \quad 30 \\
\hline
+0.5 \quad -0.7 \quad -1.1 \quad -0.7 \quad -0.3 \quad 0.0 \quad -0.5 \quad -0.9 \quad -1.8 \quad -1.3 \\
5.7 \quad 6.9 \quad 7.3 \quad 6.9 \quad 6.5 \quad 6.2 \quad 6.7 \quad 7.1 \quad 8.0 \quad 8.5 \quad 7.5 \quad 9.2 \quad 11.0 \\
75 \quad 30 \quad 12 \quad 11 \quad \quad \quad 9 \quad 10 \quad 10 \quad 17 \quad 25 \quad 100 \quad 200 \\
\hline
+0.9 \quad 0.0 \quad -0.4 \quad -0.7 \quad 0.0 \quad -0.1 \quad -1.1 \quad -0.3 \quad -1.0 \\
4.9 \quad 5.8 \quad 6.2 \quad 6.5 \quad 5.8 \quad 6.5 \quad 6.9 \quad 6.1 \quad 6.8 \\
30 \quad 27 \quad 32 \quad 15 \quad 14 \quad \quad \quad 10 \quad 11 \quad 13 \quad 30 \\
\hline
+2.9 \quad +2.4 \quad +1.3 \quad -0.2 \quad 0.0 \quad -0.2 \quad -0.5 \quad +0.7 \quad +0.5 \\
2.3 \quad 2.8 \quad 3.9 \quad 5.4 \quad 5.2 \quad 5.4 \quad 5.7 \quad 4.5 \quad 4.7 \\
30 \quad 24 \quad 18.5 \quad 13.5 \quad \quad \quad 8 \quad 9 \quad 13 \quad 30 \\
\hline
+1.8 \quad -0.9 \quad +0.2 \quad 0.0 \quad -0.2 \quad +0.7 \quad +0.9 \\
2.1 \quad 3.0 \quad 3.7 \quad 3.9 \quad 4.1 \quad 3.2 \quad 3.0 \\
30 \quad 25 \quad 21 \quad 17 \quad \quad \quad 12 \quad 25 \quad 30 \\
\hline
+2.4 \quad +1.7 \quad +1.0 \quad +0.1 \quad 0.0 \quad -0.2 \quad +0.4 \quad +1.3 \\
2.1 \quad 2.8 \quad 3.5 \quad 4.4 \quad 4.5 \quad 4.7 \quad 4.1 \quad 3.2 \\
30 \quad 21 \quad 17 \quad 15 \quad \quad \quad 12 \quad 14 \quad 25 \quad 30 \\
\hline
-0.2 \quad -0.4 \quad -0.8 \quad -0.4 \quad 0.0 \quad -0.5 \quad -0.8 \quad -0.4 \quad -0.2 \\
2.1 \quad 2.4 \quad 2.7 \quad 2.3 \quad 6.9 \quad 7.4 \quad 7.7 \quad 7.3 \quad 7.1 \\
Head \quad 27 \quad 15 \quad 12 \quad 12 \quad \quad \quad 9 \quad 11 \quad 12 \quad 30 \\
\hline
+0.2 \quad +5.9 \quad +2.9 \quad -0.8 \quad 0.0 \quad 0.0 \quad -0.1 \quad -0.4 \quad +1.1 \quad +1.6 \quad +1.0 \\
3.6 \quad 3.9 \quad 6.9 \quad 10.6 \quad 7.8 \quad 9.8 \quad 9.9 \quad 10.2 \quad 8.7 \quad 8.2 \quad 8.8 \\
30 \quad 27 \quad 20 \quad 14 \quad 13 \quad 0 \quad 7 \quad 9 \quad 13 \quad 20 \quad 30 \\
\hline
-2.0 \quad -0.6 \quad -0.9 \quad -0.3 \quad 0.0 \quad -0.2 \quad -1.1 \quad -2.8 \quad -3.3 \quad -3.6 \\
7.0 \quad 5.6 \quad 5.9 \quad 5.3 \quad 5.0 \quad 5.2 \quad 6.1 \quad 7.8 \quad 8.3 \quad 8.6 \\
30 \quad 15.5 \quad 15 \quad 13 \quad \quad \quad 7 \quad 10 \quad 20 \quad 25 \quad 30 \\
\hline
+5.7 \quad +3.9 \quad -0.5 \quad 0.0 \quad 0.0 \quad -0.2 \quad +0.6 \quad +1.5 \quad +2.4 \quad +2.7 \\
+1.8 \quad 0.0 \quad 4.4 \quad 3.9 \quad 3.9 \quad 4.1 \quad 3.3 \quad 2.4 \quad 1.5 \quad 1.2 \\
33 \quad 23 \quad 16 \quad 8 \quad \quad \quad 10 \quad 11.5 \quad 14.5 \quad 20 \quad 30 \\
\hline
+3.2 \quad +2.6 \quad -0.5 \quad -0.2 \quad 0.0 \quad -0.5 \quad -0.4 \quad -1.3 \\
1.1 \quad 1.8 \quad 4.9 \quad 5.6 \quad 4.4 \quad 4.9 \quad 4.8 \quad 5.7 \\
30 \quad 27 \quad 17 \quad 8 \quad \quad \quad 11 \quad 12 \quad 25 \quad 30 \\
\hline
-3.9 \quad +1.1 \quad -1.7 \quad +1.1 \quad +0.1 \quad 0.0 \quad 0.0 \quad +1.3 \quad -1.6 \quad -3.9 \quad -5.8 \\
9.3 \quad 9.8 \quad 7.1 \quad 4.8 \quad 5.3 \quad 5.4 \quad 4.1 \quad 1.6 \quad 9.3 \quad 11.2 \\
55 \quad 16.8 \quad 14 \quad 0 \quad 8.5 \quad 10.7 \quad \quad \quad 6.5
\end{array}$$

1236.62

245

5.2 1237.4

12.73

1247.71

1.64 1239.98

246

12.9 1234.8

+50

9.2 1238.5

247

6.7 1241.0

+75

4.7 1243.0

248

5.3 1242.4

249

5.3 1242.4

250

4.0 1243.7

L. 250+
B.M.

1.18 1246.58 (1246.52)

251

3.7 1244.0

252

3.4 1244.4

+22

12" C.I. Pipe

53.1 1244.6

4.8 1242.9

253

2.3 1245.4

12.98

1259.43

1.26 1246.75

^{-0.8} 4.0 ^{-0.4} 5.6 ^{0.0} 5.2 ^{0.0} 5.2 ^{-0.2} 5.4 ^{-0.6} 5.8 ^{-2.3} 7.5
 30 16 11 12 6 12 30

^{+4.5} 8.4 ^{+3.5} 9.4 ^{-0.9} 13.8 ^{-0.4} 13.3 ^{0.0} 12.9 ^{0.0} 13.0 ^{-0.1} 11.2 ^{+1.7} 11.2 ^{+2.7} 11.2
 30-25 20 14 12 6 10 14 25=30

^{+5.2} 4.0 ^{+4.6} 4.6 ^{-0.6} 9.8 ^{+0.2} 9.0 ^{0.0} 9.2 ^{-0.5} 9.7 ^{+0.4} 8.8 ^{+0.9} 8.3 ^{+0.4} 8.8
 30 25 15 13 0 10 12 20 30

^{+4.0} 2.7 ^{+3.6} 3.1 ^{+1.0} 5.7 ^{+0.4} 6.3 ^{-0.1} 9.8 ^{-0.5} 9.2 ^{0.0} 6.7 ^{-0.2} 6.9 ^{-0.3} 7.5 ^{-0.3} 7.0 ^{-1.2} 7.9
 30 27 22 18 16 14 6 9 12 30

^{+1.9} 2.8 ^{0.0} 4.7 ^{-1.4} 6.1 ^{-0.5} 5.2 ^{+0.2} 4.5 ^{0.0} 4.7 ^{-0.5} 5.2 ^{-1.4} 6.1 ^{-0.3} 5.0 ^{-0.7} 5.4
 30 19 16 12 5 7 10 12 30

^{+1.7} 3.6 ^{-0.1} 5.4 ^{0.7} 6.0 ^{-0.1} 5.4 ^{0.0} 5.3 ^{-0.5} 5.8 ^{-1.3} 6.6 ^{-1.0} 6.3 ^{-1.5} 6.8
 30 18 15 7 13 25 = 30

^{+0.3} 4.5 ^{+0.2} 5.1 ^{-0.2} 5.5 ^{0.0} 5.3 ^{-0.3} 5.6 ^{-0.7} 6.0 ^{-0.5} 5.8 ^{-1.7} 7.0 ^{-2.2} 7.5
 30 25 14 8 10 12 25 30

^{+2.0} 3.0 ^{+0.6} 3.4 ^{-0.1} 4.1 ^{0.0} 4.0 ^{-0.2} 4.2
 30 16 13 18 ^{+1.0} 3.0
 23 mill house

^{+1.6} 2.1 ^{+0.5} 3.2 ^{-0.6} 4.3 ^{-0.1} 3.8 ^{0.0} 3.7 ^{-0.5} 4.2 ^{-0.8} 4.5 ^{-0.2} 3.9 ^{+0.5} 3.2 ^{+0.2} 3.5
 30 18 16 11 7 10 13 25 = 30

^{+0.1} 3.3 ^{-0.5} 3.9 ^{0.0} 4.4 ^{+0.1} 4.3 ^{0.0} 3.7 ^{0.0} 3.4 ^{-1.2} 4.6 ^{-0.7} 4.1 ^{-1.5} 4.9
 30 18 17 14 9 13 14 25 = 30

^{-0.1} 3.2 ^{-1.7} 4.8 ^{-0.1} 3.2 ^{0.0} 3.1 ^{-0.5} 3.6 ^{-1.8} 4.9 ^{-2.2} 5.3 ^{-3.5} 6.6
 30 10.5 9 8.5 14.1 25 7.5

^{-0.9} 3.2 ^{-0.8} 3.1 ^{-1.1} 3.7 ^{-0.2} 2.5 ^{0.0} 2.3 ^{-0.1} 2.4 ^{-1.1} 3.4 ^{-0.5} 2.8 ^{-1.4} 3.1 ^{-1.7} 3.7 ^{0.0} 4.0
 30 14 13 10 9 11 12 16 25 30

1259.43

254

11.6 1247.8

+40

9.6 1249.8

255

5.5 1253.9

+40

4.3 1255.1

B.M. 255+60

1.48 1257.95

(1257.91)

256

6.8 1252.6

+15.5

Trp. Line

7.7 1251.7

+45

9.2 1250.2

+75

10.1 1249.3

257+05

10.7 1248.7

+15

Culvert

+35

11.0 1248.4

+65

10.8 1248.6

+95

10.5 1248.9

258+25

9.9 1249.5

+3.8	+3.0	+0.5	+0.4	-0.5	0.0	0.0	-0.4	+0.7	+1.1	+1.5
7.8	8.2	11.1	11.2	12.1	11.6	11.6	12.0	12.3	10.5	10.1
30	23	19	16	13	10	10	10	13	21	30

+5.1	+3.9	+1.6	+0.4	+1.2	0.0	0.0	-0.1	-0.3	+1.9	+1.8
4.5	5.7	8.0	9.2	8.4	9.6	9.6	9.7	9.9	7.7	7.8
30	22	16	14	12	5	11	11	12	19	30

+3.0	+1.2	+0.2	0.0	-0.3	-0.8	-0.4	-0.3	0.7
2.5	4.3	5.3	5.5	5.8	6.3	5.1	5.8	6.2
30	14	13	10	12	14.5	2.5	30	

+1.8	+0.9	+0.7	-0.9	-0.5	0.0	-0.4	-1.1	-0.4	-1.1
2.5	3.4	3.6	5.2	4.8	4.3	4.7	5.4	4.7	5.4
30	24	18	15	13	9	12	14.5	30	

+2.9	+2.1	+1.0	-0.7	0.0	0.0	-0.7	-1.1	+1.2	+1.2	+0.8
3.9	4.7	5.8	7.5	6.8	6.8	7.5	7.9	5.6	5.6	6.0
30	21	16	13.5	9	12	17	25	30		

+3.5	+3.1	+2.1	+1.0	-0.8	-0.3	0.0	-0.1	-1.1	-0.9	+1.7	+1.7
4.2	4.6	5.6	6.1	8.5	8.0	7.7	7.8	8.8	8.6	6.0	6.0
30	25	20	16	12	9	5	11	14	19	25	

9.2

10.1

10.7

11.0

10.8

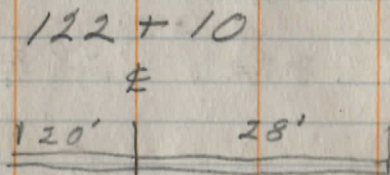
10.5

9.9

Jan. 18, 1924, Fiedler
+22°, Cloudy, Marks
Grau.

122 + ~~50~~ 46 ±

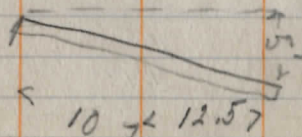
Present. 8" Vit. Pipe
Req. 12" C.I. Pipe, 60', No. H.W.S.



Req. 12" C.I. Pipe, 48', No. H.W.

114 + 00
29' Long, Stone Box O.K.

105 + 98 10" Sec. C.I. Pipe



Build Hillside 12" C.I. Pipe
± F.L. 2 1/2' Below Profile.
Dig. Outlet 100', 1' deep, 3' Wide

98 + 80

12" Sec. C.I. Pipe, Take up
+ relay on lower grade.
154' of Sid Hill H.W.S.
23 1/2' of pipe in old culvert

93 + 73.

Extent on left, 3 1/2' conc. slab top
" " Right 4' " " "

80 + 73

Culv. has been covered with
conc. slab.
Extend on left with 3' slab top
" " R. " 3' " "
Use King Hall Type
Retain as at present.

72+32.

11' span, Conc. Top
Clear Rdwy, 16'2"
1' Curb on each side.
Build Iron Rail on Curbs
+ Guard Rails on both sides
of each Approach

67+50

12" Sec. C.I. Pipe
Extend Both Ends
With ~~12"~~ C.I. Pipe.

52+35 ^{Remove 6" V.P.}
Build 12" New.

45+50, Conc. O.K

41+40, Conc. Good
Extend L. End, 3' x 2 1/4'

35+85

12" C.I. Pipe.
Extend on Left.
Build H.W.S.

1+25 10" C.I. Pipe. ~~W~~

Remove

2+25 Build 12" Encased K.P.

Use Culvert As it is

12+00 Extend, ~~4' slab top~~
~~on both ends~~

21+72 Stone Box N.G. 2x2

Build New. 3'x3'

Remove 24" Elm + 30" Elm

27+67 Remove old.

Build 3'x3'

28+10 Remove 20" Elm

125+08 Extend L. H.W. upward

134+43 O.K.

140+38 Extend on Right
by 3.0' slab top, open Bottom.

145+55 Remove Cap Stone
from E. End & place
on W. H.W. after moving
W. Cap stone inward.
Extend & Build H.W. + N.W. ^{ing} at
E. end

152+85 Stone Box, N.G.
Build std 3' x 3' conc. Box

158+46 Extend ^{5'} on Left
with 2' x 2' std. Box

160+78 Stone Box, N.G. Remove
Build 3' x 3' std. conc. Box

170+06.5 Stone Box, Remove.
Build 3' x 3' conc. box.

178+67.5 Remove Stone Box
Build 3' x 3' conc. Box

185+43 Stone Box, Retain
Extend on L. with 2' x 2' conc.

197+80 Stone Box, Remove.
Build std. 3' x 3' conc. Box

April 30 2
April 25) H. Claus, C. Rand,
D. Parks.

Sta B.S. H.I. F.S. Elev G.L.

B.M. 881				1173.72
91				1178.4
92				1178.1
93				1175.5
94				1176.0
95				1178.1
96				1181.7
97				1191.3
98				1199.2
99				1204.6
100				1208.8
B.M	9.79	1222.86		1213.07
101				1214.5
T.P	12.45	1235.10	0.21	1222.65

EAST

WEST

Grade
1904

		20.5	21.5
		19.0	20.5
		19.0	17.5
		19.0	18.5
		18.5	18.5
		17.0	19.5
		27.0	30.5
		25.5	30.0
		20.5	23.0
		14.06	13.99
		16.0	10.75
		16.0	23.0
		16.0	23.0
		8.51	0.6
		16.0	28.0

F01

F02

EAST
~~Right~~

WEST
~~Left~~

Sta	B.S.	H.I.	F.S.	Elev	G.L.				
102		1235.10		1220.9		13.20	12.40	$\frac{00.8}{18.0}$	7.72 $\frac{05.5}{28.0}$
103				1226.5		7.2	8.7	$\frac{F1.1}{15.0}$	2.75 $\frac{04.9}{28.0}$
104				1231.0		8.10	3.21	$\frac{F0.1}{17.0}$	1.7 $\frac{01.4}{21.5}$
T.P.	11.49	1249.39	2.20	1232.90					
105				1235.2		8.19	7.71	$\frac{00.5}{18.5}$	7.75 $\frac{00.5}{24.0}$
106				1239.4		3.99	3.70	$\frac{00.3}{17.5}$	4.25 $\frac{F0.7}{20.0}$
107				1241.8		1.59	2.26	$\frac{F0.7}{17.0}$	2.36 $\frac{F0.8}{17.0}$
T.P.	6.55	1249.10	1.84	1242.55					
108				1244.3		3.80	4.01	$\frac{F0.2}{18.0}$	2.80 $\frac{04.0}{14.0}$
T.P.	15.15	1261.64	2.21	1246.79					
109				1248.3		12.34	10.65	$\frac{01.7}{17.0}$	8.45 $\frac{03.9}{23.0}$
110				1253.7		6.94	6.05	$\frac{00.9}{22.0}$	4.91 $\frac{02.0}{24.0}$
B.M				1256.5					
111				1257.4		3.24	3.75	$\frac{F0.5}{20.0}$	2.54 $\frac{00.5}{22.5}$
112				1259.8		1.84	1.3	$\frac{F0.6}{21.5}$	0.14 $\frac{00.7}{23.5}$

1220.24

3,70 1265,00 0,84 1261,30

113

1259,0

5,00 2,84 ~~F1.8~~
~~6,0~~

3,14 ~~G1.9~~
~~21,5~~

114

1258,6

5,40 8,44 ~~F3,0~~
~~13,0~~

9,10 ~~F3,7~~
~~18,0~~

115

1259,4

4,60 5,95 ~~F1.4~~
~~17,5~~

5,79 ~~F1.2~~
~~14,5~~

116

1262,1

1,90 2,92 ~~F1.5~~
~~17,0~~

0,51 ~~G1.4~~
~~22,0~~

T.P.

3,77 1267,78 0,96 1267,04

T.P.

5,41 1262,37

EAST

~~Right~~

WEST

~~Left~~

50

S.W. corner Parcel 118t E side of Road

May 3, 1928 D. Parks, C. Rand, H. Clause

B.M.	B.S.	H.I.	F.S.	Elev	G.L.
	8.48	1116.69		1108.21	
1				1111.20	
2				1112.00	
3				1112.80	
4				1114.95	
T.P.	12.04	1127.24	1.49	1115.20	
5				1118.45	
6				1121.84	
7				1124.45	
8				1126.16	
9				1126.81	
T.P.	3.80	1129.84	1.20	1126.04	

Grade	Post	W. Root	20" Hickory	R
5.49	4.04	$\frac{C1.5}{22.5}$	4.91	$\frac{F1.4}{17.0}$
4.69	4.20	$\frac{C0.7}{25.0}$	6.81	$\frac{F2.1}{19.0}$
3.89	3.82	$\frac{C0.1}{20.5}$	6.13	$\frac{F2.2}{17.0}$
1.74	1.82	$\frac{F0.1}{20.0}$	3.81	$\frac{F1.6}{18.0}$
8.79	7.81	$\frac{C1.0}{22.0}$	9.23	$\frac{F0.4}{20.0}$
5.40	3.11	$\frac{C2.3}{23.5}$	5.40	$\frac{0.00}{20.0}$
2.79	1.55	$\frac{C1.2}{22.0}$	4.20	$\frac{F1.4}{19.5}$
1.08	0.84	$\frac{C0.2}{19.5}$	2.30	$\frac{F1.2}{18.5}$
0.43	0.47	$\frac{F0.1}{19.5}$	0.91	$\frac{F0.5}{19.5}$

18 1172,72
 19 1136,75
 20 1136,31
 T.P. 3,82 1137,27 8,91 1133,21

Record B, M 1,51 1137,28 1,51 1136,17 1136,16

21 1133,97
 22 1137,38
 T.P. 12,24 1149,42 0,50 1137,18
 23 1142,77
 24 1146,18
 T.P. 3,54 1150,86 2,10 1147,32
 25 1145,67

5,97 5,44 $\frac{C0,5}{21,5}$ 4,01 $\frac{C1,9}{23,5}$
 6,41 7,91 $\frac{F0,5}{18,5}$ 5,12 $\frac{C1,3}{22,0}$
 8,22 9,14 $\frac{F0,9}{18,5}$ 9,56 $\frac{F1,3}{18,0}$

SE, Root 30" Maple Left 20+40

3,71 2,90 $\frac{C0,8}{21,5}$ 5,21 $\frac{F2,1}{16,5}$
 0,30 3,25 $\frac{F3,6}{19,5}$ 6,25 $\frac{F6,4}{23,0}$
 6,45 2,86 $\frac{C1,8}{20,0}$ 3,62 $\frac{C3,6}{26,0}$
 2,64 0,83 $\frac{C1,5}{25,5}$ 0,93 $\frac{C1,7}{23,0}$
 5,19 2,29 $\frac{C2,9}{25,0}$ 4,46 $\frac{C0,7}{20,5}$

115026

26.

1141,70

T.P

1.45 1140,17 12.14 1138,72

27

113282

28

1138,04

T.P

9.26 1145,53 3.90 1136,27

29

1142,34

T.P

10.24 1155,79 0.08 1145,45

30

1147.23

T.P

9.57 1162,83 2,53 1153,26

Record
B.M.

1158,56
3,35 1159,48

9,14

8,47

C0,7
22,0

9,11

C0,1
19,5

2,35

6,35

F4,0
18,5

8,19

F5,8
21,5

2,13

5,70

F3,6
18,0

8,23

F4,1
22,0

3,19

4,70

F1,5
18,0

2,06

C1,1
22,0

8,56

7,93

C3,6
27,5

6,21

C1,8
27,0

B.M.	5.64	1141.81		1136.17
21				1139.97
22				1137.38
T.P.	7.54	1149.35	0.00	1141.81
23				1142.77
24				1146.18
25				1145.67
26				1141.70
T.P.	2.69	1143.45	8.59	1140.76
27				1137.82
28				1138.04
29	15.99	1159.38	0.00	1143.45
				1142.34
30				1147.23
30+50				1149.49
31+50				1152.90
B.M.		0.80		1158.58

May 7, 1928 Mark D. Parks, C. Rand ⁵⁵

B.M.	S.E. Root	30" Maple	35' L. 20+40	
	7.84	7.05	$\frac{C 0.8}{21.5}$	9.97 $\frac{F 2.1}{16.5}$
	4.43	8.02	$\frac{F 3.6}{19.5}$	10.82 $\frac{F 6.4}{23.0}$
	6.58	2.33	$\frac{C 4.3}{26.0}$	2.97 $\frac{C 3.6}{26.0}$
	3.17	+0.2	$\frac{C 3.4}{25.5}$	0.91 $\frac{C 2.3}{25.5}$
	3.68	4.88	$\frac{C 2.9}{25.0}$	3.00 $\frac{C 0.7}{20.5}$
	7.65	6.98	$\frac{C 0.7}{22.0}$	7.67 $\frac{C 0}{19.5}$
	5.63	9.70	$\frac{F 4.1}{18.5}$	11.50 $\frac{F 5.9}{21.5}$
	5.41	9.01	$\frac{F 3.6}{18.0}$	11.56 $\frac{F 6.1}{22.0}$
	1.11	2.23	$\frac{F 1.5}{18.0}$	0.00 $\frac{C 1.1}{22.0}$
	12.15	8.54	$\frac{C 3.6}{27.5}$	10.93 $\frac{C 1.7}{23.0}$
	9.89	6.54	$\frac{C 3.4}{24.0}$	8.64 $\frac{C 1.3}{22.0}$
	6.48	1.52	$\frac{C 5.0}{27.0}$	5.70 $\frac{C 0.8}{25.0}$
	N. root, Maple,	L 31.50	Rec.	1158.56

2.34 1160.90 1158.56

32 1154.66

33 1155.27

34 1155.00

35 1154.00

35+85 Culvert.

36 1153.88

37 1155.55

38 2.86 1163.42 0.34 1160.56 1158.00

38+95 1159.22

40 1157.98

41 1156.23

B.M. 8.97 1163.46 8.97 1154.45 1154.47

42 1156.43

B.M. L. 31+50

6.84 1.72 $\frac{C 5.1}{27.0}$ 4.43 $\frac{C 2.4}{25.0}$

5.63 6.65 $\frac{F 1.0}{19.0}$ 7.79 $\frac{F 2.2}{18.0}$

5.90 3.87 $\frac{C 2.0}{22.5}$ 7.13 $\frac{F 1.2}{19.0}$

6.90 7.94 $\frac{F 1.0}{16.5}$ 9.34 $\frac{F 2.4}{17.0}$

1158.95 ^{6.75} 9.95 $\frac{C 3.0}{30.0}$ 1150.35 ^{9.55} 10.55 $\frac{C 1.0}{30.0}$

7.62 9.09 $\frac{F 2.1}{17.0}$ 9.27 $\frac{F 2.3}{17.0}$

5.35 7.65 $\frac{F 2.3}{16.5}$ 6.88 $\frac{F 1.5}{17.0}$

2.90 1.35 $\frac{C 2.6}{23.0}$ 1.35 $\frac{C 1.6}{22.0}$

4.20 0.27 $\frac{C 3.9}{24.5}$ 2.81 $\frac{C 1.4}{24.5}$

5.52 4.78 $\frac{C 0.7}{20.0}$ 4.42 $\frac{F 1.9}{17.0}$

7.19 9.95 $\frac{F 2.8}{18.0}$ 9.88 $\frac{F 2.7}{17.0}$

X, N.W. Cor., W. Head-wall, 41+40, Rec. 1154.49

7.03 7.84 $\frac{F 0.8}{17.0}$ 7.33 $\frac{F 2.3}{17.0}$

1163.46

43 3.38 1160.08 1158.50 4.96

5.28 1165.36

44 1160.50 4.86

45 1160.50 4.86

5.73 1159.63
1159.58 Record

B.M. 9.53 1169.11

46 1159.77 9.34

47 1160.94 8.17

48 1163.89 5.22

49 1166.34 2.77

T.P. 5.97 1174.14 0.94 1168.17

50 1167.91 6.23

51 1168.59 5.55

52 1168.50 5.64

117 C 3.8
25.5

0.26 C 4.6
27.5

F 2.0
17.0

X on N.W. cor., W. Headwall, 45 + 50

May 9, 1922. P. Parks, C. Road

F 1.1
18.0
14.0

F 1.9
16.5
14.0

F 2.4
17.0

C 2.1
21.0

C 3.9
25.0

F 1.9
17.5

F 2.6
17.0

338 C 1.6
23.0

2.52 C 2.3
20.5

7.85 F 3.0
15.5

11.41 F 2.1
E 16.0
17.0

10.38 F 2.2
16.0
17.0

6.30 F 1.1
16.0

0.62 C 2.1
22.5

7.82 C 1.4
20.5

7.78 F 2.2
16.0

7.92 F 2.3
17.0

1174.14

52+35 Culvert

1164.84 $\frac{7.80}{9.30} \frac{C1.5}{30}$ 1162.16 $\frac{9.98}{11.98} \frac{C2.0}{30}$

53 1168.30 5.84 5.84 $\frac{0.0}{20.0}$

7.75 $\frac{F1.9}{16.0}$

54 1168.10 6.04 4.24 $\frac{C1.8}{22.0}$

6.46 $\frac{F0.4}{18.5}$

55 1167.90 6.24 4.10 $\frac{C2.1}{23.5}$

6.91 $\frac{F0.7}{19.5}$

56 1167.70 6.44 5.50 $\frac{C0.9}{21.0}$

6.37 $\frac{F0.1}{19.0}$

57 X 1167.50 6.64 6.68 $\frac{0.4}{F1.1} \frac{C0.5}{18.5}$

6.13 $\frac{C0.5}{19.5}$

B.M 4.08 1170.06

Nail S.E. Root 15" Maple 25' Left Sta 57+10

0.62 1170.60 1169.98 Record

58 1167.30 3.30 4.74 $\frac{F1.4}{17.5}$

5.31 $\frac{F2.0}{16.0}$

59 1167.00 3.60 5.59 $\frac{F2.0}{16.0}$

4.78 $\frac{F1.2}{17.0}$

60 1165.99 4.61 6.96 $\frac{F2.4}{16.0}$

6.27 $\frac{F1.7}{16.0}$

61 1164.27 6.33 7.79 $\frac{F1.5}{17.0}$

8.01 $\frac{F1.7}{16.0}$

62 1162.45 8.15 7.99 $\frac{C0.1}{20.5}$

7.90 $\frac{C0.3}{20.5}$

1170.60

T.P. 2.73 1142.77 10.56 1160.04

63 1160.63 2.14 2.07 $\frac{C0.1}{19.0}$ 0.35 $\frac{C1.8}{22.0}$

64 1158.31 3.96 3.88 $\frac{C0.1}{18.5}$ 1.56 $\frac{C8.4}{23.5}$

65 1156.70 6.07 7.90 $\frac{F1.8}{17.0}$ 5.68 $\frac{C0.4}{20.0}$

66 1154.00 8.77 10.19 $\frac{F6.4}{17.5}$ 8.92 $\frac{F0.2}{19.5}$

T.P. 1.70 1153.26 10.61 1152.16

67 1151.56 2.30 5.12 $\frac{F2.3}{17.5}$ 5.27 $\frac{F3.0}{17.5}$

67+50 Culvert 1146.78 $\frac{5.07}{7.08}$ $\frac{CB0}{35.5}$ 1145.30' $\frac{7.06}{8.56}$ $\frac{C1.5}{21.5}$

68 1150.25 3.61 5.85 $\frac{F2.2}{17.5}$ 6.44 $\frac{F2.8}{17.5}$

B.M. 0.14 0.51 1153.35
0.14 1153.49 1153.35 record

Nail on E. roof 20" maple Lt. Sta 68+80
Stake driven by E root of maple

69 1148.44 5.05 2.53 $\frac{C2.5}{24.0}$ 0.61 $\frac{C4.4}{23.0}$

70 1144.50 8.99 5.34 $\frac{C3.7}{26.0}$ 4.85 $\frac{C4.1}{23.0}$

1153.49

T.P. 11.27 1142.22

71 0.03 1142.25 1139.50 2.75 3.77 $\frac{F1.0}{18.0}$ 0.03 $\frac{C2.7}{23.5}$ 72 1135.68 6.57 10.44 $\frac{F3.9}{19.0}$ 8.62 $\frac{F2.1}{18.5}$

T.P. 8.29 1142.18 8.36 1133.89

73 1136.44 5.74 8.63 $\frac{F2.9}{18.0}$ 9.76 $\frac{F4.0}{18.5}$ 74 1140.82 1.36 5.77 $\frac{F4.4}{20.0}$ 3.20 $\frac{F1.8}{18.0}$

T.P. 11.84 1153.77 0.23 1141.95

75 1145.42 8.37 8.91 $\frac{F0.5}{19.0}$ 4.25 $\frac{C4.1}{27.0}$

T.P. 9.04 1162.68 0.15 1153.64

76 1150.02 12.66 6.46 $\frac{C6.2}{31.0}$ 6.75 $\frac{C5.2}{30.0}$ 77 1153.77 8.91 3.14 $\frac{C5.8}{30.0}$ 7.04 $\frac{C4.9}{23.0}$ 78 1154.20 8.48 7.53 $\frac{C1.0}{22.5}$ 8.75 $\frac{F0.3}{20.5}$

1162.68

79 1152.07

T.P. 1.58 1154.68 9.64 1153.02

80 1150.86

B.M. 8.93 1158.99 4.46 1150.14 1150.06 record

81 1151.19

82 1153.05

83 1156.00

T.P. 12.51 1171.09 0.41 1159.58

84 1159.08

85 1162.00

86 1165.00

87 1168.00

May 10 1928 D. Burks C. Rand

10.61 9.12 $\frac{C1.5}{23.0}$ 9.14 $\frac{C1.5}{22.5}$

3.74 6.50 $\frac{F2.8}{17.5}$ 7.30 $\frac{F3.6}{18.5}$

x on S.W. Cor W. Headwall Stone Culv. ^{STB} 80+25

7.80 11.34 $\frac{F3.5}{18.5}$ 11.24 $\frac{F3.4}{18.5}$

5.91 10.07 $\frac{F4.7}{19.5}$ 8.72 $\frac{F2.8}{18.5}$

2.99 0.33 $\frac{C2.7}{25.0}$ 2.23 $\frac{C0.8}{21.5}$

12.09 6.62 $\frac{C5.5}{29.0}$ 9.95 $\frac{C2.1}{24.0}$

9.09 6.06 $\frac{C3.0}{27.5}$ 7.66 $\frac{C1.7}{22.5}$

6.09 5.51 $\frac{C0.6}{21.5}$ 5.74 $\frac{C0.4}{21.0}$

3.09 2.91 $\frac{C0.2}{21.5}$ 3.42 $\frac{F0.3}{19.5}$

T.P. 10.26 1171.09 1180.25 1.10 1169.99

88 1171.00 9.25 9.45 $\frac{F0.2}{19.0}$ 10.51 $\frac{F1.3}{17.0}$

B.M 6.38 1180.20 6.48 1173.77 1173.72 Record

89 1174.00 6.20 5.86 $\frac{C0.8}{23.0}$ 7.48 $\frac{F1.3}{16.0}$

90 1176.52 3.68 4.27 $\frac{F0.6}{20.0}$ 2.18 $\frac{C1.5}{23.5}$

T.P. 4.67 1183.27 1.60 1178.60

91 1178.08 5.19 2.91 $\frac{C2.3}{24.5}$ 5.38 $\frac{F0.2}{20.5}$

92 1178.66 4.61 4.71 $\frac{F0.1}{20.5}$ 5.12 $\frac{F0.5}{17.8}$

93 1178.28 4.99 8.12 $\frac{F3.1}{17.5}$ 8.24 $\frac{F3.3}{19.0}$

T.P. 6.16 1181.45 7.98 1175.29

93+73 Culvert

94 1178.57 2.88 6.64 $\frac{F3.8}{18.5}$ 6.66 $\frac{F3.8}{19.0}$

$\frac{F0.2}{19.0}$ 10.51 $\frac{F1.3}{17.0}$

Nail on W. root 24" Maple Rt. Sta 88+40

6.20 5.86 $\frac{C0.8}{23.0}$ 7.48 $\frac{F1.3}{16.0}$

3.68 4.27 $\frac{F0.6}{20.0}$ 2.18 $\frac{C1.5}{23.5}$

5.19 2.91 $\frac{C2.3}{24.5}$ 5.38 $\frac{F0.2}{20.5}$

4.61 4.71 $\frac{F0.1}{20.5}$ 5.12 $\frac{F0.5}{17.8}$

4.99 8.12 $\frac{F3.1}{17.5}$ 8.24 $\frac{F3.3}{19.0}$

X on middle of East Head Wall.

2.88 6.64 $\frac{F3.8}{18.5}$ 6.66 $\frac{F3.8}{19.0}$

1181,95

95 1181,14

0,31 4,06 $\frac{F3,8}{18,5}$ 3,58 $\frac{F3,8}{18,5}$

T.P 14,05 1194,94 0,56 1180,29

96 1186,00

8,94 8,93 $\frac{0,0}{17,5}$ 9,75 $\frac{F0,8}{17,0}$

T.P 13,86 1204,97 3,83 1191,11

97 1192,00

12,97 5,35 $\frac{C7,6}{30,5}$ 8,91 $\frac{C4,1}{27,0}$

98 1198,00

$\frac{2,13}{6,97}$ 0,9 0,40 $\frac{C7,6}{30,0}$ 8,05 4,84 $\frac{C3,2}{26,5}$

T.P 13,04 1216,94 1,07 1203,90

98+80 Culvert

1202,70 $\frac{8,24}{14,24}$ $\frac{C6,0}{33}$ 1199,5 $\frac{12,94}{17,44}$ $\frac{C4,5}{33}$

99 1204,00

12,94 10,15 $\frac{C2,8}{23,0}$ 12,43 $\frac{C0,5}{20,5}$

B.M. 3,85 1213,09

Nail in W. root 24" Evergreen 40' Rt $5^{\circ} 9' 10''$

3,85 1216,92 1218,07 record

100 1210,00

6,92 4,86 $\frac{C2,2}{23,0}$ 8,06 $\frac{F1,1}{15,0}$

T.P 10,66 1226,52 1,06 1215,86

101 1216,00

10,52 4,29 $\frac{C6,2}{28,0}$ 12,08 $\frac{F1,6}{16,0}$

1226.52

102 3.86 1222.66 1222.00
10.44 1233.10

103 1227.85

T.P. 12.04 1242.62 2.52 1230.58

104 1232.65

105 1236.40

106 1240.00

106+00 Culvert

T.P. 11.51 1253.60 0.53 1242.09

107 1243.60

108 1247.20

109 1250.80

4.52 11.10 5.74 $\frac{C5.7}{28.0}$ 4.52 3.86 $\frac{C0.7}{18.0}$

5.25 0.62 $\frac{C4.6}{28.0}$ 6.72 $\frac{F1.5}{15.0}$

9.97 9.28 $\frac{C0.7}{21.5}$ 10.79 $\frac{F0.8}{17.0}$

6.22 4.05 $\frac{C2.2}{24.0}$ 6.00 $\frac{C0.2}{18.5}$

2.62 1.97 $\frac{C0.7}{20.0}$ 2.94 $\frac{F0.3}{19.5}$

1238.01 $\frac{1.11}{4.61}$ $\frac{C3.5}{31}$ 1236.70 $\frac{3.27}{4.27}$ $\frac{C3.0}{59}$

10.00 11.51 $\frac{F1.5}{17.0}$ 11.66 $\frac{F1.7}{17.0}$

6.40 8.57 $\frac{F2.2}{18.0}$ 7.34 $\frac{F0.9}{17.0}$

2.20 0.44 $\frac{C2.4}{23.5}$ 2.66 $\frac{C0.4}{17.0}$

1255,60

T.P. 10.32 1261A3 2,49 1256,11

100 1254,40 7,03 5,91 $\frac{C1,1}{22,0}$ 4,77 $\frac{C2,3}{24,0}$

B.M. 4,93 1256,50 record

2 Nail 1 1/2 W. root 50" Elm 35' Pt Sta 110 + 25

7,17 1263,64

111 1257,42 6,22 4,62 $\frac{C1,6}{22,5}$ 5,83 $\frac{C0,4}{20,0}$
112 1259,26 4,38 2,21 $\frac{C2,2}{23,5}$ 3,37 $\frac{C1,0}{21,5}$
113 1259,90 3,74 2,69 $\frac{C1,1}{21,5}$ 5,58 $\frac{F1,8}{14,0}$

TP 9,23 1266,51 6,36 1257,28

6,54 10,68 $\frac{F4,1}{18,0}$ 10,05 $\frac{F3,5}{15,0}$
114 1259,97 4,51 7,38 $\frac{F1,0}{17,5}$ 7,58 $\frac{F2,1}{17,0}$
115 1264,00 3,76 2,13 $\frac{C1,6}{22,0}$ 4,64 $\frac{F0,9}{18,0}$

114 1259,97

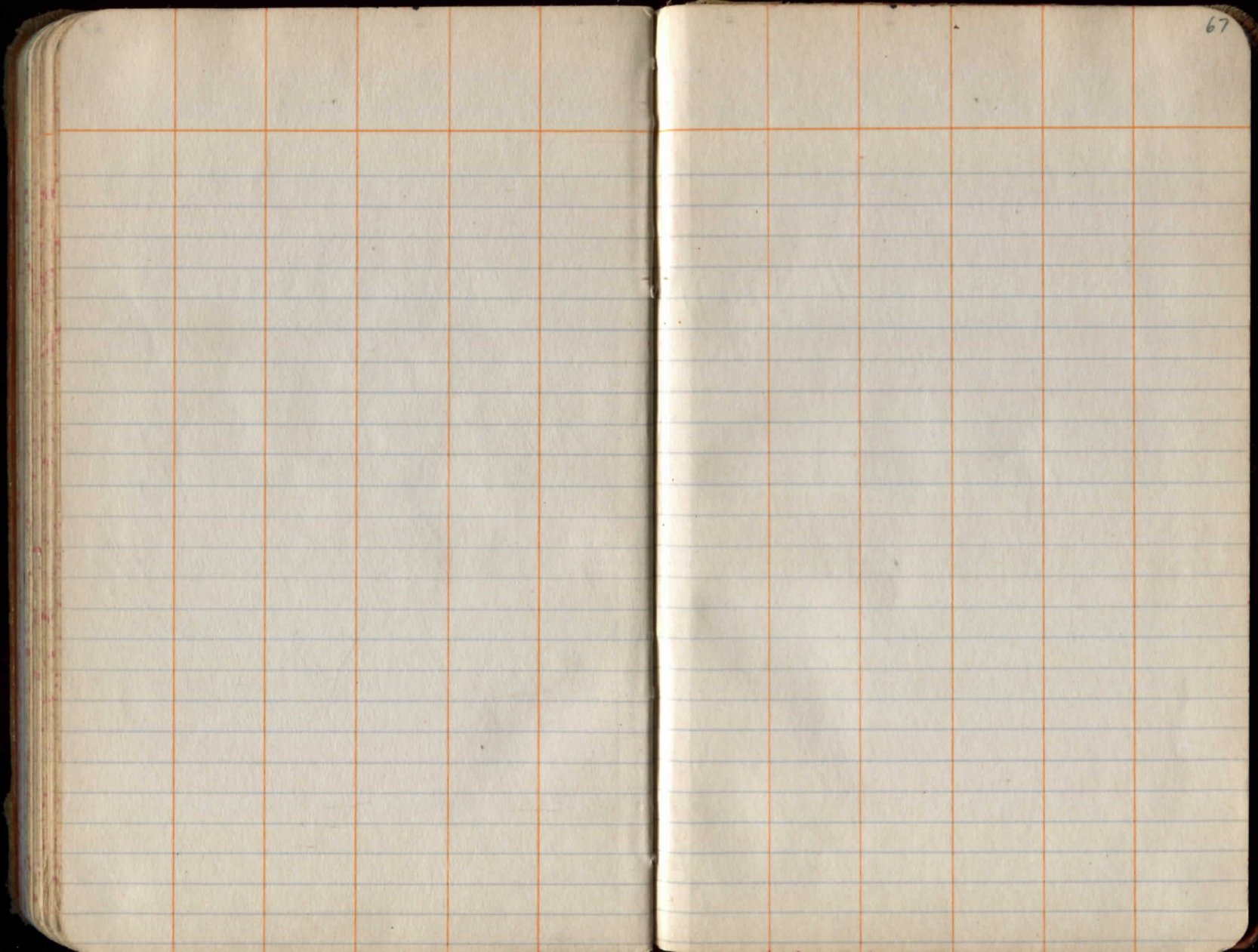
115 1264,00

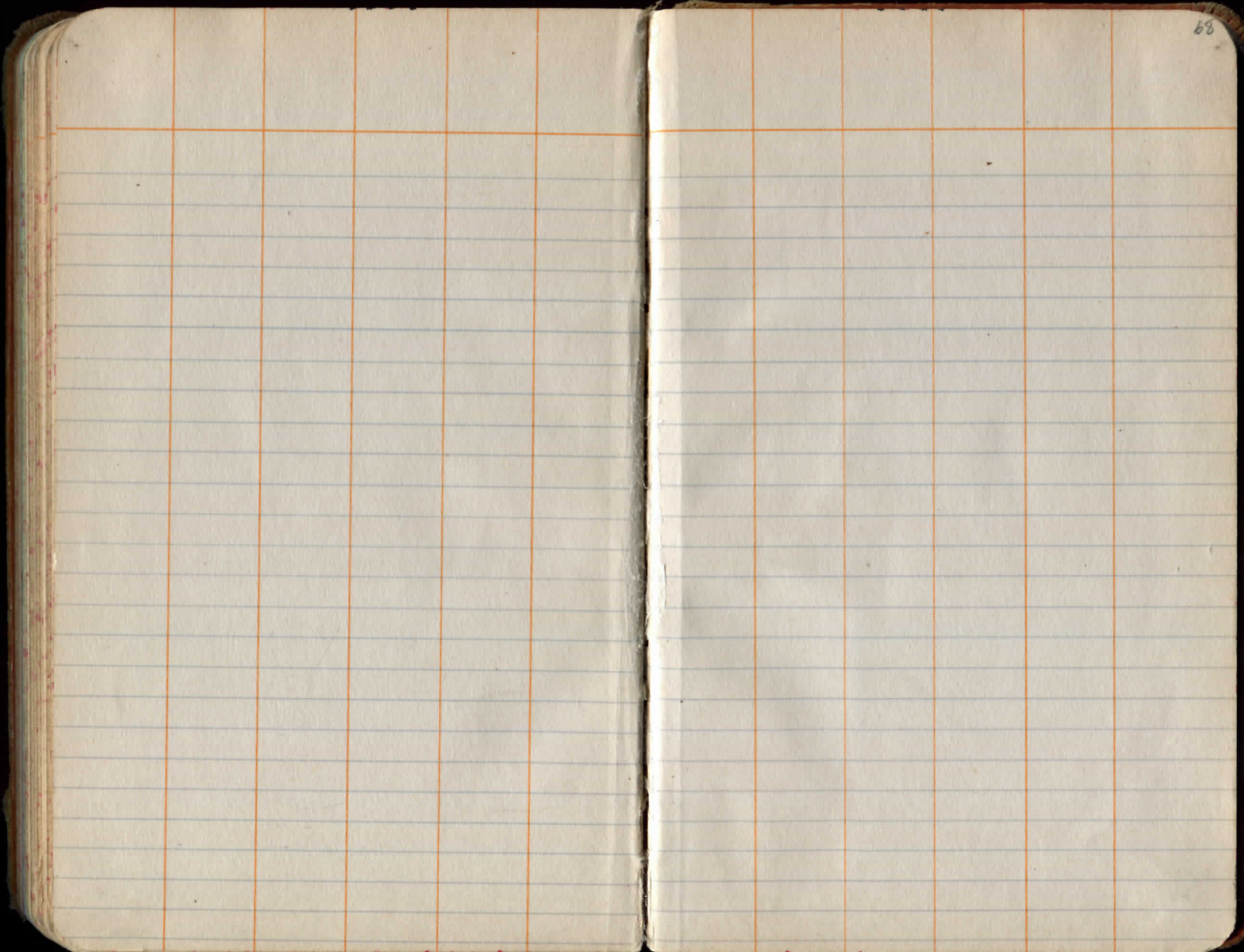
116 1262,75

T.P. 7,89 1269,01 5,09 1264,12

T.P. 6,70 1262,31

S.W. Cor. Cat. Porch 118 + E side of road





B.M 7.49 1115.70 1108.21

2725 Culvert

B.M, 2.59 1138.71 1132.17

21+72 Culvert

B.M 5.14 1141.81 1136.17

T.P 7.54 1149.35 0.00 1141.81

T.P 0.00 1140.76 8.59 1140.76

27+67 Culvert

4-9-29 Kiedler - Steeley - 32° Pine

31+50 +2.11 1160.67 ^{B.M} 1158.56

T.P -12.54 1148.13

+0.15 1148.28

T.P -12.66 1135.62 ^{N.W. corr. W. Pipe}

+1.53 1137.45

fl. line inlet 6.78 1130.67 ^{27+67 =}

outlet 15' N. of culv. inlet 7.28 ^{1 1/2 6" tile}

" 7.84 1129.61 ^{fl. line}

" 6.65 ^{1 1/2 6" tile}

10' N.W. of culv. inlet 7.21 1130.24 ^{fl. line}

" 7.21 1130.24 ^{fl. line}

next pg

30.67
1129.61
1.06

76

W. Root 20" Hickory Right of Sta 0+00

1110.0 ^{2.2}/_{5.7} ^{63.5}/₃₀ 1108.5 ^{6.2}/_{7.2} ^{61.0}/₃₀

S. E Root 30" Maple 35' Left 20+40

1128.9 ^{7.81}/_{9.81} ^{62.0}/₃₀ 1127.2 ^{9.11}/_{11.11} ^{62.0}/₃₀

S. E Root 30" Maple 35' L 20+40

1129.87 ^{8.89}/_{10.89} ^{68.0}/₃₀ 1127.27 ^{9.09}/_{11.09} ^{68.0}/₃₀

N.W. corr. W. Parahet +1.50 1137.42

Outlet of culvert 7.39 1130.03 ⁽²⁷⁻⁶⁷⁾

" " 150' E. of 9.0 1128.4 ditch

" " 110' W. 9.9 1127.5

Board.

11	4	meals	2 bed	<u>10.00</u>
12	4	"	"	<u>2.40</u>
				Pd. <u>6.00</u>
14	6	"	3 "	<u>4.50</u>
15	9	"	3 "	<u>6.00</u>
16	9	"	3 "	<u>6.00</u>
17	6	"	"	<u>3.00</u>
				<u>19.50</u>

12	livery			<u>5.00</u>
17	"			
16	telephone			.10

22	6	meals	3 bed	<u>4.50</u>
23	5	"	"	<u>2.50</u>
				<u>7.00</u>

6.00
 19.50
 7.00

 32.50

B.M. At Huntsburg = x on

S.W. cor. Concrete Porch
to Store. Elev = 1260.20

B.M. at Huntsburg Twp.'s

S-line - Two nails in
W. root 20" hickory 40' Rt.
Sta. 147+80. Elev = 1108.21

PLEASE RETURN TO
 GAUGA COUNTY ENGINEER
 COURT HOUSE

CHARDON O.
 PHONE 256-4X

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
21	3.46 6 in.	41	6.76 6 in.	61	10.06 6 in.	81	13.36 6 in.				
22	3.63 0	42	6.93 0	62	10.23 0	82	13.53 0				
23	3.79 6	43	7.09 6	63	10.39 6	83	13.69 6				
24	3.96 0	44	7.26 0	64	10.56 0	84	13.86 0				
25	4.12 6	45	7.42 6	65	10.72 6	85	14.02 6				
26	4.29 0	46	7.59 0	66	10.89 0	86	14.19 0				
27	4.45 6	47	7.75 6	67	11.05 6	87	14.35 6				
28	4.62 0	48	7.92 0	68	11.22 0	88	14.52 0				
29	4.78 6	49	8.08 6	69	11.38 6	89	14.68 6				
30	4.95 0	50	8.25 0	70	11.55 0	90	14.85 0				
31	5.11 6	51	8.41 6	71	11.71 6	91	15.01 6				
32	5.28 0	52	8.58 0	72	11.88 0	92	15.18 0				
33	5.44 6	53	8.74 6	73	12.04 6	93	15.34 6				
34	5.61 0	54	8.91 0	74	12.21 0	94	15.51 0				
35	5.77 6	55	9.07 6	75	12.37 6	95	15.67 6				
36	5.94 0	56	9.24 0	76	12.54 0	96	15.84 0				
37	6.10 6	57	9.40 6	77	12.70 6	97	16.00 6				
38	6.27 0	58	9.57 0	78	12.87 0	98	16.17 0				
39	6.43 6	59	9.73 6	79	13.03 6	99	16.33 6				
40	6.60 0	60	9.90 0	80	13.20 0	100	16.50 0				

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

75.71
 1.99
 73.72

64' Diameter
 100
 2.00

1116.70
 1110.0
 5.70

1115.7
 1108.5
 7.2

